

# Multidirectional understanding of chiral structure on the honeycomb sandwich composite sheet: Control sensing of density

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**Abstract.** This study used a modified orthotropic elastic shell model to study the vibration of chiral single-walled carbon nanotubes. Budiansky and Sanders (1963) are the source of the stress and strain equations. Both the impact of height-to-diameter ratios and boundary conditions are included in this model. The governing equations are expressed in eigenform using the complex approach. The fundamental frequencies of SWCNTs are obtained by solving this eigenform using MATLAB software. The impact of density and boundary conditions on frequency behavior is examined. For chiral nanotubes, the frequency pattern with two boundary conditions seems to be parallel. As density increased, the frequencies dropped. Frequencies will be higher with a higher index. Compared to the equivalent C-F situation, the C-C frequencies are higher. There is a significant frequency shift between the C-C and C-F boundary condition curves for shorter tubes and shorter chiral indices. This frequency study is anticipated by the author for high frequencies in intriguing electromagnetic devices.

**Keywords:** boundary conditions; chiral SWCNTs; computer software; density variation; nano-sized structures; orthotropic model

## 1. Introduction

CNTs are effective for moving fluids and gases due to their cylindrical mechanism and exceptional mechanical properties. The main tool for continuum mechanics (Qi *et al.* 2024, Zhang *et al.* 2023) is its computational capacity to generate results of large range systems. Various models provide significant computing efficiency and accuracy, making them a viable choice for further research in vibration field (Yang *et al.* 2025a, Wang *et al.* 2023). Kroto *et al.* (1985) and associates discovered Buckminster Fullerene, or C<sub>60</sub>, a novel kind of carbon molecule. Ru (2000) investigated the bending of carbon nanotubes using a multilinear model. The mechanical behavior of different materials is explored by Xu *et al.* (2023) and Yang *et al.* 2025b. Wang *et al.* (2005) investigated the limitations and uses of the multiwalled carbon nanotubes.

Wang (2005) investigated the vibration of carbon nanotubes using the shell model. The bending of multi-walled carbon nanotubes is described using a multi-elastic shell model. Experimental and numerical studies are observed by Zhang *et al.* (2024) and Yu *et al.* (2022). Reddy (2007) updated the nonlocal relation beam ideas found in the body of current literature. A simpler Flugge shell for the vibration

of double-walled carbon nanotubes was presented by Natsuki *et al.* (2008). These tubes are completely submerged in liquid. The interaction of van der Waals forces as two exclusive beams was clearly demonstrated by the free vibrations of double-walled carbon nanotubes (Xu *et al.* 2008). The nested CNT tubes with double walls were modeled by Xu *et al.* (2008) as individual elastic beams. According to their research, double-walled CNT remained unchanged under specific edge conditions at a given invariable frequency. Ke *et al.* (2009) examined the free nonlinear vibrations of double-walled carbon nanotubes (CNTs) using nonlocal Timoshenko beam theory, and they used differential quadrature approach to derive frequency equations. For multi-walled carbon nanotubes with nonlinear geometric and physical consequences for nonlinear vibrations of tubes, Adali (2009) suggested the principle of variation. Shima (2011) and Wang *et al.* (2006) demonstrated carbon nanotube buckling. The investigation's primary focus was on small-scale diameters and aspect ratios, which demonstrated the applicability of Donnell shell theory for vibration analysis. The buckling analysis of carbon nanotubes was studied by Chandrasekhar *et al.* (2009) and Hollerer and Celigoj (2013) using an atomistic approach and the Cosserat rod model. The continuum elastic energy is parameterized and produced. Liu *et al.* (2025) and Ni *et al.* (2024) investigated shear effect of composite plates and interlayer of Cu nanoparticles. Hu *et al.* (2012) and Budarapu *et al.* (2014) taking into account the continuum bars for carbon nanotube vibrations. The frequency vibrations of chiral double-walled CNT were

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demonstrated by Chemi *et al.* (2015). Nonlocal Euler Bernoulli beam theory was utilized to model the set of governing equations. Peng *et al.* (2025) and Gao *et al.* (2023) utilized the sequence table for composite laminated plate and inspiration for bionic bimanual robot teleoperation. Bouadi *et al.* (2018) developed a new model displacement field for the nonlocal buckling properties of a single graphene sheet. The Eringen relation was used for the theoretical formation with the length scale parameter. Li *et al.* (2024) and Cong *et al.* (2024) investigated shear wave ultrasonography and composite cylindrical shells. Fatahi-Vajari *et al.* (2019) investigated the torsional vibration of SWCNTs using second order PDEs. These equations are reduced by GT, and the torsional frequency equation is then generated using HPM. Malikan and Eremeyev (2020) predicted the buckling analysis of CNTs using the Winkler matrix with different boundary conditions. The Hamilton's notion was used to measure the carbon nanotubes' hardness and softness-stiffness. Alves *et al.* (2023) and Qiu *et al.* (2024) investigated the control of soft robotic hands and diesel engine damper design.

Pourasghar *et al.* (2021) demonstrated the transient heat conduction and vibration of SWCNTs based on Eringen's and heat conduction theories. The energy scale is found using the nonlocal term with heat conduction theory. Zhang *et al.* (2023) and Su *et al.* (2023) investigated heterogeneous random porous materials and concealable grippers. Wang *et al.* (2023, 2025) investigated the plastic deformation of calcareous sand and the wrinkling monitoring of metal tubes using nonlocal elasticity theory. Simsek (2010) used nonlocal EBM with supported edge situations to determine the forced vibration of SWCNTs. For effects, aspect ratio and velocity are carefully calculated. Moreover, the excitation frequency and load velocity have a significant impact on the nanostructures.

Madihav *et al.* (2011) developed the model that was utilized in conjunction with the Timoshenko and Euler Bernoulli beam theories using a harmonic balanced approach. They introduced the two-way vibrational behavior and the Timoshenko beam model of single-walled carbon nanotubes. Additionally, they investigated how van der Waal forces affected the frequency spectra of medium and nearby double-walled carbon nanotubes.

Both Zhang *et al.* (2025) and Zou *et al.* (2024) investigate the dispersion of Lamb waves and dual-loop control of QUAV trajectory. Lei *et al.* (2012) took into consideration surface effects in conducting vibration of double-walled carbon nanotubes using the Timoshenko beam model and nonlocal theory. The significance of surface effects and nonlocality, with the largest modes of vibration in shorter tubes is utilized. In 2022, Ghasemi and Gouran assessed the vibration of SWCNTs lying on the Pasternak foundation and filled with fluid. For pipe flow, He *et al.* (2024) and Cai *et al.* (2025) employed particle-based absorber-roller systems and Lagrangian particle models.

Different researcher used different techniques for material investigations (Samaniego *et al.* 2020, Zhuang *et al.* 2021, Penna 2023, Civalek *et al.* 2023, Barretta *et al.* 2022, Civalek and Baltacıoğlu 2018, Benvenuti and Simone 2013,

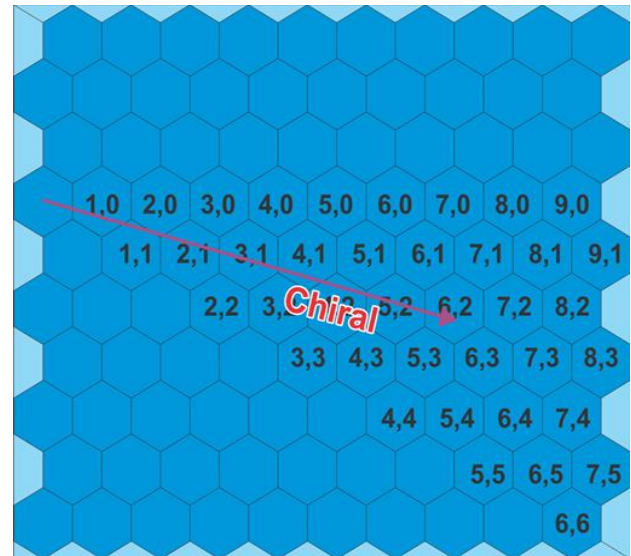


Fig 1 The graphene sheet showing chiral SWCNTs schematically

Safaei *et al.* 2019, Benmansour *et al.* 2019, Akbaş 2020, Forsat *et al.* 2021, Luo *et al.* 2022, Moradiet *al.* 2023, Hussain 2024, Hussain *et al.* 2017, Hussain 2020, 2022, Alghaffari *et al.* 2023, Qazaq *et al.* 2022, Ghandourah *et al.* 2023, 2024, Taj *et al.* 2023, Hussain *et al.* 2023, Khedher *et al.* 2023, 2024, Hussain *et al.* 2024).

In order to determine the natural frequencies against density under clamped-clamped (C-C) and clamped-free boundary conditions, the current study is used for vibration of chiral SWCNTs. MD simulations demonstrated that the parameters is appropriately selected, and the findings of this model are in good agreement with those of the Timoshenko beam model and beam element. MATLAB coding has been used to obtain the frequency equation's eigen solutions. The current thorough findings might also be useful in designing the basic frequencies of nanostructures.

## 2. Mathematical formulation

Because of different radii in different structure, two types of carbon nanotube configurations are found: single-walled carbon nanotubes (SWCNTs) and multi-walled carbon nanotubes (MWCNTs). A graphene sheet is considered SWCNTs once it has been rolled once to form a cylinder with an end cape. Fig. 1 shows the graphene sheet with a schematic representation of chiral SWCNTs. In this case, the axial coordinate is  $x$ , and the angular coordinate is  $\theta$ . Axial displacement is denoted by  $u$ , circumferential displacement by  $v$ , and inward deflection by  $w$ . The density is denoted by  $\rho$ . In the longitudinal direction,  $\nu_x$  is the Poisson ratio, and in the circumferential direction,  $\nu_\theta$ .  $R$  is the radius of the carbon nanotubes, and  $h$  is the tube's thickness.

The longitudinal modulus of elasticity is denoted by  $\epsilon_x$ , while the circumferential modulus is represented by  $\epsilon_\theta$ . Similarly  $\nu_x$  is poisson's ratio in longitudinal direction and  $\nu_\theta$  s in circumferential direction.

2.1 Strain-displacement relationships

The strain-displacement relations from Budiansky and Sanders (1963) theory are furnished as

$$\begin{aligned} \varepsilon_x &= \frac{\partial u}{\partial x} \\ \frac{\partial v}{R\partial\theta} - \varepsilon_\theta &= \frac{w}{R} \\ \gamma_{x\theta} - \frac{\partial u}{R\partial\theta} &= \frac{\partial v}{\partial x} \end{aligned} \tag{1}$$

The stress and strain relationship is given as

$$\begin{aligned} \frac{(1 - \nu_x \nu_\theta)}{(\varepsilon_x + \nu_x \varepsilon_\theta)} &= \frac{E_x}{\sigma_x} \\ \frac{(1 - \nu_x \nu_\theta)}{(\varepsilon_\theta + \nu_\theta \varepsilon_x)} &= \frac{E_\theta}{\sigma_\theta} \\ \tau_{x\theta} &= \gamma_{x\theta} G_{x\theta} \end{aligned} \tag{2}$$

The axial and circumferential prestresses are

$$\begin{aligned} N_\theta &= \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma_\theta dz \\ N_x &= \int_{-\frac{h}{2}}^{\frac{h}{2}} \sigma_x dz \\ N_{x\theta} &= \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{x\theta} dz. \end{aligned} \tag{3}$$

Furthermore longitudinal and circumferential Poisson ratios and Young's moduli are denoted by  $\nu_x$ ,  $\nu_\theta$  and  $E_x$ ,  $E_\theta$  respectively. The four parameters  $E_x$ ,  $\nu_x$ ,  $a$ , and  $\beta$  can be used to characterize the orthotropic elastic shell model. Additionally,  $D_x$ ,  $D_\theta$ , and  $D_{x\theta}$ , respectively, reflect effective bending stiffness (Pablo *et al.* 2003, Sirenko *et al.* 1996). The mathematical formulation can be seen (Taj and Zhang 2011). The three-equation orthotropic elastic shell model that was created (Eslami and Javaheri 1999) describes the forces that cause the vibration of chiral SWCNTs.

$$\begin{aligned} &\left[ (K_x + N_x)R^2 \frac{\partial^2}{\partial x^2} + 2RN_{x\theta} \frac{\partial^2}{\partial x \partial \theta} \right] u \\ &+ \left[ \frac{K_{x\theta}R^2 + D_{x\theta}}{R^2} + N_\theta \right] \frac{\partial^2}{\partial \theta^2} \\ &+ \left[ R(\nu_x K_\theta + K_{x\theta}) \frac{\partial^2}{\partial x \partial \theta} \right] v \\ &+ \left[ -R(\nu_\theta K_x - N_\theta) \frac{\partial}{\partial x} + \left[ RD_x \frac{\partial^3}{\partial x^3} - \frac{D_{x\theta}}{R} \frac{\partial^3}{\partial x \partial \theta^2} \right] \right] w = 0 \end{aligned} \tag{4}$$

$$\left[ R(\nu_\theta K_x + K_{x\theta}) \frac{\partial^2}{\partial x \partial \theta} \right] u \tag{5}$$

$$\begin{aligned} &+ \left[ (K_\theta + N_\theta) \frac{\partial^2}{\partial \theta^2} + 2RN_{x\theta} \frac{\partial^2}{\partial x \partial \theta} \right] v \\ &+ \left[ -R(\nu_\theta K_x - N_\theta) \frac{\partial}{\partial \theta} - 2RN_{x\theta} \frac{\partial}{\partial x} + \left[ (v_\theta D_x + 3D_{x\theta}) \frac{\partial^3}{\partial x^2 \partial \theta} \right] \right] w = 0 \end{aligned}$$

$$\begin{aligned} &\left[ R(\nu_\theta K_x - N_\theta) \frac{\partial}{\partial x} - RD_x \frac{\partial^3}{\partial x^3} + \frac{D_{x\theta}}{R} \frac{\partial^3}{\partial x \partial \theta^2} \right] u \\ &+ \left[ (K_\theta + N_\theta) \frac{\partial}{\partial \theta} + 2RN_{x\theta} \frac{\partial}{\partial x} \right] v \\ &+ \left[ -R^2 D_x \frac{\partial^4}{\partial x^4} + 2RN_{x\theta} \frac{\partial^2}{\partial x \partial \theta} \right. \\ &\quad \left. - (2v_\theta D_x + 4D_{x\theta}) \frac{\partial^4}{\partial x^2 \partial \theta^2} \right] w = 0 \\ &+ \left[ \frac{D_\theta}{R^2} (\frac{\partial^2}{\partial \theta^2} + 1)^2 + N_\theta \frac{\partial^2}{\partial \theta^2} \right. \\ &\quad \left. + N_x R^2 \frac{\partial^2}{\partial x^2} - K_\theta \right] w = 0 \end{aligned} \tag{6}$$

Here CNTs are supported as simply supported, the vibration analysis of free CNTs is considered by the solution of the form,

$$u(x, \theta, t) = \alpha_m U(x) \cos n \theta e^{i\omega t} \tag{7}$$

$$v(x, \theta, t) = \beta_m V(x) \sin n \theta e^{i\omega t} \tag{8}$$

$$w(x, \theta, t) = \gamma_m W(x) \cos n \theta e^{i\omega t} \tag{9}$$

where amplitudes in longitudinal, circumferential, and radial directions are represented by the constants  $U$ ,  $V$ , and  $W$ , respectively. In the axial direction,  $m$  is the half wave number and  $L$  is the tube's length.

$k_m$  is the wave vector in longitudinal direction.  $\omega$  is the angular frequency and  $n$  is the circumferential wave number.

$$U(x) = \cos k_m x$$

$$V(x) = W(x) = \sin k_m x$$

where

$$k_m = \frac{m\pi}{L} \quad \text{(C-C)} \tag{10}$$

$$k_m = (2 \frac{m-1}{2L})\pi \quad \text{(C-F)}$$

Putting (10) into (2), the eigen value form is attained.

3. Results and discussion

Here, the deep analysis of carbon nanotubes is studied using the orthotropic elastic shell model. With the current model, the impacts of density against fundamental frequencies are found.

The first step in determining the vibration characteristics

Table 1 Analyzing frequency levels with Duan *et al.* (2007)

		$f$ (THz)					
Aspect ratio		5.26	5.62	5.99	6.35	6.71	7.07
Clamped-clamped	Duan <i>et al.</i> (2007)	0.975	0.887	0.809	0.741	0.681	0.628
	Present	0.965	0.881	0.799	0.733	0.671	0.618
Clamped-free	Duan <i>et al.</i> (2007)	0.212	0.188	0.167	0.150	0.136	0.123
	Present	0.201	0.179	0.159	0.139	0.126	0.111

Table 2 Analyzing frequency levels with Arghavan and Singh (2011)

		$f$ (THz)				
Mode No.		1	2	3	4	5
Clamped-clamped	Arghavan and Singh (2011)	0.4323	0.4323	1.0582	1.0582	1.2661
	Present	0.4311	0.4311	1.0569	1.0573	1.2647
Clamped-free	Arghavan and Singh (2011)	0.0746	0.0746	0.4316	0.4316	0.6296
	Present	0.0732	0.0732	0.4301	0.4301	0.6281

Table 3 Analyzing frequency levels with Zhang *et al.* (2009)

		$f$ (THz)				
Aspect Ratio		21.06	24.66	28.85	31.85	35.53
MD simulation (Zhang <i>et al.</i> 2009)		0.07629	0.05798	0.04578	0.03662	0.03052
Present		0.07618	0.05786	0.04560	0.03654	0.03039

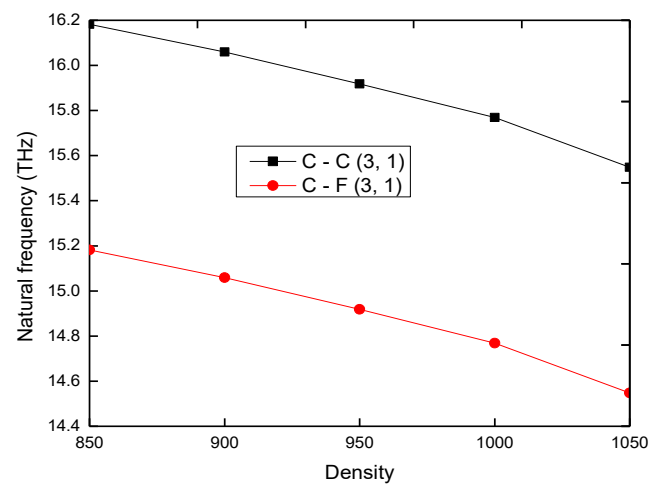


Fig. 2 Chiral (3, 1) SWCNTs' density effects on (C-C, C-F) frequencies

of chiral (3, 1), (5, 2), and (7, 3) SWCNTs using a continuum model is to validate the results with Duan *et al.* (2007), Arghavan and Singh (2011), and Zhang *et al.* (2009) to ensure accuracy as indicated in Tables 1-3. The frequencies for two distinct boundary conditions—one with a fixed diameter and length and the other parameters with a changing mode number. The frequencies is found to be in closed agreement. Following validation, it seems to have

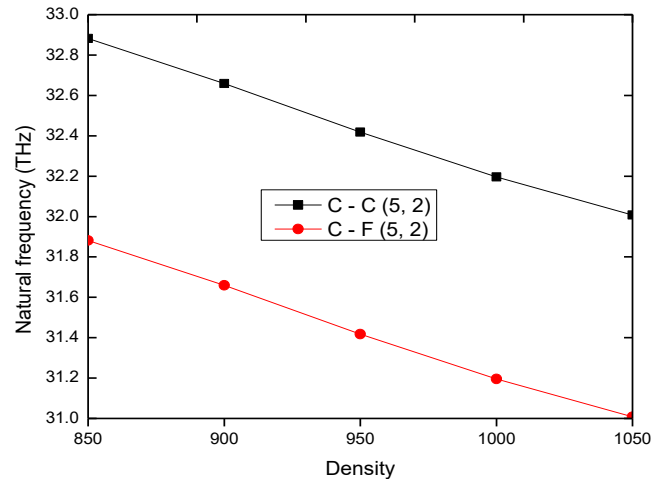


Fig. 3 Chiral (5, 2) SWCNTs' density effects on (C-C, C-F) frequencies

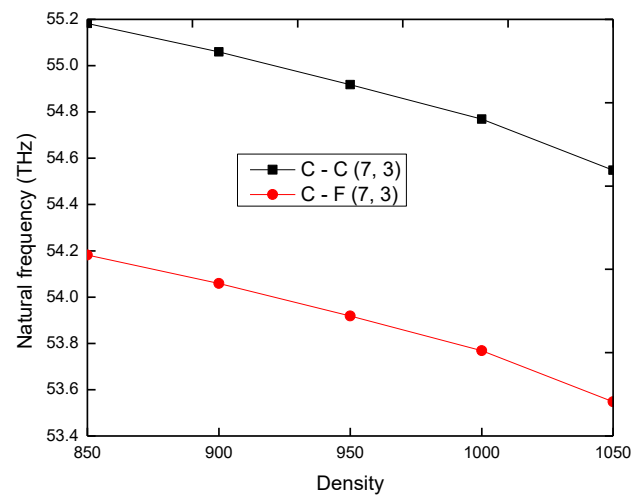


Fig. 4 Chiral (7, 3) SWCNTs' density effects on (C-C, C-F) frequencies

outstanding accuracy. The current model's results offer a potent method for examining the behavior of SWCNTs. Figs. 2-4 illustrate how vibrating chiral (3, 1), (5, 2), and (7, 3) single-walled carbon nanotubes affect density variation. The calculated results from present model for chiral index C - C (= 3, 1) at  $\rho$  (=850, 900, 950, 1000, 1050), the first nine frequencies are 16.182, 16.059, 15.918, 15.769, 15.548 and for chiral index C - C (= 5, 2), the frequencies are 32.882, 32.659, 32.418, 32.196, 32.008 and frequencies for chiral index C - C (= 7, 3), are 55.182, 55.059, 54.918, 54.769, 54.548. The frequency at which the system resonates is the nanotube's inherent frequency. Two elements contribute to the natural frequency in this case: the mass and the stiffness of the nanotube, which serves as a spring. The mass of the chiral single-walled carbon nanotubes is inversely correlated with the vibration frequencies. So due to increase of density results the decrease in resonance frequency. As a result, natural frequencies likewise fall. We turn next to examine in more detail chiral index C - F (= 3, 1) at  $\rho$  (= 850 ~ 1050) the first none frequencies are 15.182, 15.059, 14.918, 14.769, 14.548, and for chiral index C - F (= 5, 2), the frequencies are

31.882, 31.659, 31.418, 31.196, and for chiral index C - F (= 7, 3), are 54.182, 54.059, 53.918, 53.769, 53.548. The C-F boundary condition shows a similar pattern of frequencies decreasing as density increases. It is evident that the frequencies for the C-C, C-F (3, 1), (5, 2), and (7, 3) chiral indices drop off quite quickly. The chiral indices (3, 1), (5, 2), and (7, 3) all exhibit the same fall in frequency pattern. However, as the index rises from (3, 1) to (5, 2) and (7, 3), the frequencies rise as well.

For two boundary conditions, the chiral index (5, 2) lies between the chiral indexes (3, 1) and (7, 3). Furthermore, was concluded that the chiral index (3, 1) has a smaller frequency gap than the other two indexes. Compared to the C-C condition, the C-F border condition occurs less frequently. It is quite evident that the density of nanotubes significantly affects the shell's inherent frequencies. It has been shown that when density grows, so do natural frequencies. The frequencies drop with increasing density. This is primarily due to the system's mass having the opposite effect on the natural frequency.

#### 4. Conclusions

For the vibration properties of chiral single-walled carbon nanotubes, theoretical formulations based on the extended orthotropic shell model are investigated. In order to extract the frequencies of CNTs, the governing equation of motion and boundary conditions are expressed in the form of an eigenvalue using a complicated approach. Compared to the previous approaches, this improved model is less complicated. The effect of density, boundary conditions for chiral (3, 1), (5, 2) and (7, 3) on the frequencies are calculated. It is observed that the increment in the density, the frequencies decreases for chiral tubes. Both clamped-clamped and clamped-free end situations exhibit these frequency fluctuations. For general density values, the frequency pattern appears to be parallel with the two specified boundary constraints. The frequency curves with the lowest results are also observed when the density of the C-F boundary condition is changed. However, it has a significant impact on the tubes' distortion. The current frequencies are compared with several models using carefully selected parameters. It is evident from the comparisons that the current model can produce results that are suitable for frequency prediction.

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