

Accuracy improvement in motion tracking of tennis balls using nano-sensors technology

Shuning Yan^{*1}, Chaozong Xiang² and Li Guo³

¹Sports Department of Hubei Polytechnic University, Huangshi, 435003 Hubei, China

²College of physical education and health, Chongqing Metropolitan College of Science and Technology, Yongchuan, 402167 Chongqing, China

³Manufacturing Management Department, DONGFENG-CITRO AUTOMOBILE COMPANY LTD, Wuhan, 430050, Hubei, China

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Abstract. Tracking the motion of tennis balls is a challenging task in using cameras around the tennis court. The most important instance of the tennis trajectory is the time of impact and touch the court which in some cases could not be detected precisely. In the present study, we aim to present a novel design of tennis balls equipped with nano-sensors to detect the touch of the ball to the court. In the impact instance, tennis ball receives significant acceleration and change in the linear momentum. This large acceleration could deform a small-beam structure with piezoelectric layer to produce voltage. The voltage could further be utilized to produce infrared waves which could be easily detected by infrared detection sensors installed on the same video cameras or separately near the tennis court. Therefore, the exact time of the impact could be achieved with higher accuracy than image analyzing method. A detailed dynamical property of such sensors is discussed using nonlinear beam equations. The results show that within the acceleration range of tennis ball during an impact, the piezoelectric patches of the nano-sensors in the tennis ball could produce enough voltages to propagate infrared waves to be detected by infrared detectors.

Keywords: composite beam structure; impact instance; nano-sensors; Tennis ball tracking

1. Introduction

Tennis ball play is an important and luxuries sport in the world which attracts many players and fans around the world. The amount of prize in this game is higher than other sports and this makes the point count during a match very critical (Habibi *et al.* 2016, 2018a, b, 2019a, b, d, e, Esmailpoor Hajilak *et al.* 2019, Pourjabari *et al.* 2019, Safarpour *et al.* 2019a, Zhu *et al.* 2022). Especially because of the tennis ball speed the exact moment of touching the court is barely possible with naked eye (Habibi *et al.* 2017, 2019a, c, Safarpour *et al.* 2018a, 2019b, 2020, Alipour *et al.* 2020, Ebrahimi *et al.* 2020a, Ghazanfari *et al.* 2020, Chen *et al.* 2022a). Therefore, the image processing technology has helped the referees to make fair decisions for challenging points. However, the image processing method has their problems in recognizing exact moment of ball impact on the play court. Several improvements on the image processing technology have been proposed but the exact impact time determination is still suffering from mathematical approximations (Cao *et al.* 2021a, b, Yang *et al.* 2021, Li *et al.* 2022, Zhao and Wang 2022, Zhou *et al.* 2022). On the other hand, improvement is vision technologies are highly expensive. Therefore, other methodologies should be adopted on this matter.

Melo *et al.* (2021) presented a mathematical approximation algorithm to find the position of the ball

touching the court. They utilized two cameras in the tennis court to recognize both ball and court. Their main focus was developing simple and low cost embedded system for detecting trajectory which the experimental tests had approved the accuracy and efficacy of the proposed methodology. Archana and Geetha (2015) proposed an image processing approach to detect ball trajectory and players position in broadcast tennis videos. They claimed that their approach improved the accuracy on the ball track detection. Yan *et al.* (2014) developed a methodology based on machine learning method to annotating tennis game using two levels of processing. The audio processing determines the time of the impact of ball to the court and classification method for labelling sequences. They also provided experimental validation of the approach. Yong *et al.* (2011) improved a motion detection algorithm to assist users in tennis play annotation. Four different detectors had been used to evaluate their performance. It was concluded that the presented method is effective in motion detection of tennis ball. To reduce the cost of speed measurement of tennis balls, Zhao *et al.* (2019) utilized sensor technology. Using sensors on the tennis racket they successfully improved the accuracy of speed measurement about 11%. Conaire *et al.* (2009) utilized cameras to track the tennis ball. Further, the metadata obtained used to find about the sequences of events during play and position of the players. They discussed the applicability of these metadata in coaching players. These studies indicate that using cameras and image processing techniques requires improvements to be reliable and expense for improvement are very high. Thus, other technologies from different fields could be beneficial in this regard.

*Corresponding author, Ph.D.,
E-mail: yanshuning@cqcst.edu.cn

Nanotechnology has influenced many fields of technology since the superior characteristics of nano-structured materials have been recognized (Li *et al.* 2017, Zhou *et al.* 2020b, Ma *et al.* 2021, Tang *et al.* 2021, Zheng *et al.* 2021, Wang *et al.* 2022b). Nanosensors are one of the widespread usage of mechanical nanostructures (Ebrahimi *et al.* 2019b, Al-Furjan *et al.* 2020g, 2021, Shokrgozar *et al.* 2020a, Wen *et al.* 2020, Habibi *et al.* 2021b, Shariati *et al.* 2021). Nanosensors are employed as motion and vibration sensors. Using single or double layers of piezoelectric materials could convert the motions and small oscillations into electrical voltage whose amount is proportional to the deflection. Nano- and micro-beams with tip mass equipped by piezoelectric layers are prevalent in motion sensors (Kargarnovin *et al.* 2007, Arefi 2018, Shokrgozar *et al.* 2019, Mao *et al.* 2020, Shi *et al.* 2020). Using of piezoelectric layers in sandwich micro-structures is either for induce vibration or to control vibrations in beam structure (Burdess and Fawcett 1992, Bendine *et al.* 2016, Karimiasl *et al.* 2019). Because of small-scale of these sensors and their constituents, the theories of large scale materials which are examined and verified in macro-scales are proven to be insufficient in small scales. Burdess and Fawcett (1992) experimentally explored the performance of piezoelectric materials in controlling forced and free vibrations. Beam structure with cutouts was investigated by Eltahir *et al.* (2020). The nonlocal elasticity theory was employed to observe the responses of small-scale beam under static and dynamic loadings. Effects of cutouts geometry and scale of the beam on the mechanical performance were reported in detail. Bruant and Proslie (2016) reported the effect of subsized piezoelectric location on the vibration control of the functionally graded beams. They demonstrated that it is possible to use smaller piezoelectric patches with high controlling effects maintaining that the location of the piezoelectric patch should be optimized. Nadal and Pigache (2009) formulated electromechanical behavior of piezoelectric materials using Hamilton's principle. They validated the formulation of homogenous and inhomogeneous piezoelectric structures by comparing finite element results with experimental outcomes (Ebrahimi *et al.* 2019b, c, 2020b, Hashemi *et al.* 2019, Moayedi *et al.* 2019, Mohammadgholiha *et al.* 2019, Mohammadi *et al.* 2019, Habibi *et al.* 2020, Moayedi *et al.* 2020a, b, Oyarhossein *et al.* 2020b, Shariati *et al.* 2020a, b, Shokrgozar *et al.* 2020b).

In most of the sandwich micro-beams one or more layers of carbon nanotube reinforced nanocomposites (CNT-RC) are used. In addition to CNT, graphene platelets are popular reinforcements. She *et al.* (2018) reviewed the reported properties of graphene platelets and their composite. Using Eringen's nonlocal theory, Barretta *et al.* (2018) the static deflection of a nano-beam was calculated using numerical methods. They used bi-Helmholtz kernel in the integral form of nonlocal theory. There are several elasticity models incorporating small-scale effects namely strain gradient theory (Lam *et al.* 2003), couple stress theory (Hadjesfandiari and Dargush 2011), nonlocal strain gradient theory (Jirásek 2004) and other modified theories on the basis of these models. Utilizing nonlocal strain gradient theory, Li *et al.* (2015) studied wave propagation

in small scale functionally graded beams and they reported that the effects of nonlocal and material parameters are more significant in high wavenumbers. Influence of temperature in nonlocal structures were examined by Ebrahimi *et al.* (2016). They found that temperature distribution pattern has significant effect on the wave propagation in these structures. Numerical methods has proven to be effective in obtaining materials responses under static and dynamics loads (Nejad *et al.* 2016, Safarpour *et al.* 2018b, Amelirad and Assempour 2019, Al-Furjan *et al.* 2020h, Oyarhossein *et al.* 2020a, Amelirad and Assempour 2021). The complicated form of nonlocal and gradient models' differential equations necessitates using numerical approaches. One of the most effective numerical method is differential quadrature method (DQM) and its modified developments. This theory has proven to have high performance in solving nonlinear differential equations and it is widely used in solving structural mechanics problems because of presenting accurate results in comparison to analytical solutions.

In the present study, we aim to present a novel design of tennis balls equipped with nano-sensors to detect the touch of the ball to the court. In the impact instance, tennis ball receive significant acceleration and change in the linear momentum. This large acceleration could deform a small-beam structure with piezoelectric layer to produce voltage. The voltage could further be utilized to produce infrared waves which could be easily detected by infrared detection sensors installed on the same video cameras or separately near the tennis court. Therefore, the exact time of the impact could be achieved with higher accuracy than image analyzing method. A detailed dynamical property of such sensors is discussed using nonlinear beam equations. The results show that within the acceleration range of tennis ball during an impact, the piezoelectric patches of the nano-sensors in the tennis ball could produce enough voltages to propagate infrared waves to be detected by infrared detectors.

2. Methodology

The main idea in the present study is to propose a low cost and reliable methodology using nano-beam sensor technology. Micro-beam structures are extremely low weight (~1-10 milligrams) and could be mounted inside tennis balls without significantly change in its weight. Moreover, due to small cross section of the beams it will not change the mechanical properties and responses of the tennis ball. A schematic representation of a new tennis ball equipped with nano-beam sensor is depicted in Fig. 1. The nano-beam sensor is illustrated in this figure. The beam constructed using three layers of one CNT-TC composite layers and two piezoelectric layers. Viscosity effects of the high pressure gas inside the ball is modeled using viscoelastic layer in this structure. At the end of the beam, an infrared transmitter is installed which is fed by piezoelectric voltage. One side of the transmitter faces outward. This mechanism enables the nanosensors to convert deflection into infrared waves. Only transverse displacement of the beam base could induce enough

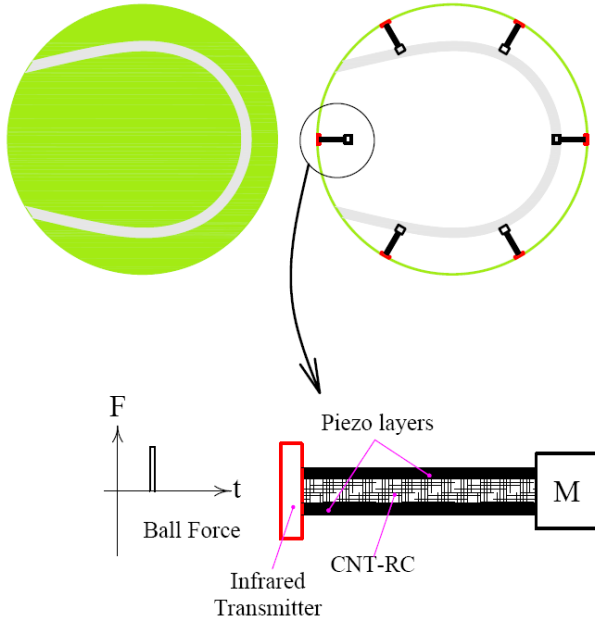


Fig. 1 Structure of cantilever nano-beam sensor and its mount inside tennis ball

deflections in the piezoelectric layers to produce voltage. Since the direction of the impact is not known, several nano-sensors should be used to ensure having enough deflection in some beams to produce infrared waves (Cao *et al.* 2020, Chen *et al.* 2022b, Fang *et al.* 2022, Wang *et al.* 2022c, Zhao *et al.* 2022). The displacement and force on the tennis ball in the case of impacts could be modeled with Kronecker Delta function as below:

$$d_{y_l} = d\delta(t - t_0) \quad (1)$$

In this relation, d_{y_l} is the displacement of the end of cantilever beam along local y coordinate system which normal to the axis of the beam.

As a moderate to heavy impact loads hits the ball, a sudden change in the linear momentum of the ball is changes abruptly resulting in abrupt displacement in beam base. This base excitation load cause deflection in the beam based on the flexural properties and amount of the tip mass. Therefore, the flexural properties and mass value are two main parameters to be designed for having enough deflection. The deflection should produce instant voltage in piezoelectric layers and the properties of this layer should be such that produces infrared beam in transmitters. The property of the piezoelectric is another parameter have to be determined. In addition, this loading condition should not produce oscillation in nano-beam for a long time (greater than 1 millisecond). If so, the infrared beam will continue to transmit even after the impact. Thus the viscoelastic layer should be designed so that the beam falls into near critical damping condition. This is another parameter to investigate.

Having transmitted infrared waves, it is possible to install infrared receivers around the tennis court as shown in Fig. 2. To avoid extra numbers of transmitter, they are only installed along court lines which are important in annotations. There are total 20 numbers of the sensors all sending signals to a server to be used alongside image

processing cameras for detecting exact moment of ball impact.

3. Mathematical formulation

3.1 Kinematic of the nano-beam sensor

As discussed in introduction section, the classical theory is insufficient for model small-scale structures. Therefore, we employ strain gradient theory for modeling the deformable constituent of the structure. The strain tensor \mathbf{E} in small displacement and deflection is expressed as below (Hashemi *et al.* 2019, Al-Furjan *et al.* 2020c, d, e, f, Bai *et al.* 2020, Cheshmeh *et al.* 2020, Li *et al.* 2020a, Lori *et al.* 2020, Najaafi *et al.* 2020, Shariati *et al.* 2020c, Xiong *et al.* 2020, Guo *et al.* 2021b, Liu *et al.* 2021a):

$$\mathbf{E} = \frac{1}{2}(\nabla\mathbf{u} + \nabla^T\mathbf{u}) \quad (2)$$

in which \mathbf{u} is the displacement vector. Assuming Bernoulli-Euler beam theory the components of the displacement in local coordinate system could be described as (Adamian *et al.* 2020, Al-Furjan *et al.* 2020a, b, Li *et al.* 2020b, Liu *et al.* 2020b, Zare *et al.* 2020, Dai *et al.* 2021b, Habibi *et al.* 2021a, He *et al.* 2021, Huang *et al.* 2021a, Liu *et al.* 2021b, Zhang *et al.* 2021):

$$\begin{aligned} u_{x_l}(x_l, y_l, z_l, t) &= -y_l \frac{\partial w(x_l, t)}{\partial x} \\ u_{y_l}(x_l, y_l, z_l, t) &= w(x_l, t) \\ u_{z_l}(x_l, y_l, z_l, t) &= 0 \end{aligned} \quad (3)$$

The subscript l denotes local coordinate system. Variables u_{i_l} for $i = x_l, y_l, z_l$ are displacement along x , y and z local axes. Transverse deflection of the beam is denoted by $w(x_l, t)$. Using this relations, the nonzero components of strain tensor are:

$$E_{xx} = -y_l \frac{\partial^2 w(x_l, t)}{\partial x^2} \quad (4)$$

The bonding between layers in sandwich beam is assumed to be perfect. Here, we are not seeking details of the formulations as it is presented in several articles comprehensively for an account please refer to (Lam *et al.* 2003, Akgöz and Civalek 2011, Ebrahimi and Barati 2017)

3.2 Kinetics of nano-beam sensor

Hamilton's principle is a powerful method based on the different types of energies in structures which is employed to obtain equations of motion of nano-beam with tip mass. The form of this equation is (Liu *et al.* 2020a, Wang *et al.* 2020, Zhou *et al.* 2020a, Dai *et al.* 2021a, Guo *et al.* 2021a, Shao *et al.* 2021, Wu and Habibi 2021, Kong *et al.* 2022):

$$\int_0^t (\delta U - \delta K - \delta W) dt = 0 \quad (5)$$

In which U is the sum of strain energy in the structure, K is the total kinematic energy and W is the work done by external forces. The δ operator represents the variation of

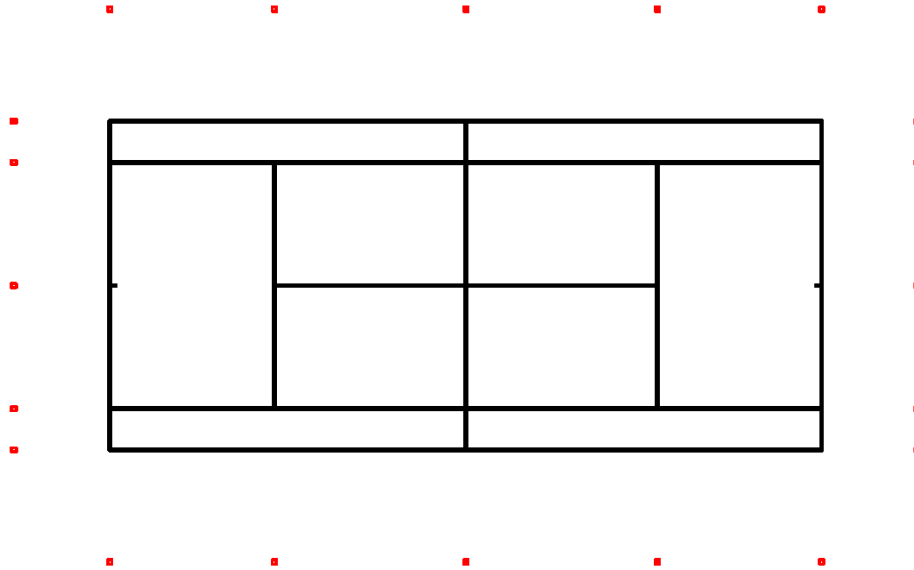


Fig. 2 Location of infrared detectors around tennis court.

the variable. In the following the expression for kinetic is given (Ma *et al.* year, Zhao *et al.* year, Hou *et al.* 2021, Huang *et al.* 2021b, c, Jiao *et al.* 2021, Liu *et al.* 2021c, Moradi *et al.* 2021, Xu *et al.* 2021, Dong *et al.* 2022, Luo *et al.* 2022, Michael *et al.* 2022, Wang *et al.* 2022d, Yang *et al.* 2022, Yu *et al.* 2022):

$$K = \int_0^L \sum_{i=1}^N \frac{1}{2} \rho_i A_i \left[\frac{\partial w(x_i, t)}{\partial t} \right]^2 dx_i + \frac{1}{2} M \left[\frac{\partial w(L, t)}{\partial t} \right]^2 \quad (6)$$

The length of the beam is L and concentrated tip mass is equal to M . Moreover, N shows numbers of different materials used in the sandwich beam structure, ρ is mass density and A is cross section of each layer. The expression for strain energy is as follows:

$$U = b \int_{-c}^c \int_0^L T_{xx} E_{xx} dx_l dy_l \quad (7)$$

In which, T_{xx} is the normal stress component along local x axis and b is the width of the beam. In addition, c is the half of the beam cross section height. External work on the structure is defined as:

$$W = F d_{y_l} \quad (8)$$

In which the concentrate force F is not known in this case.

3.3 Constitutive equations

In the strain gradient theory, it is assumed that the stress in material point depends on the both strain state and the gradient of strain at that point. The gradient of strain incorporates the effects of strain in neighborhood of the material point into account. The tensorial form of the strain gradient equations is as follows (Fan *et al.* 2022, Wang *et al.* 2022a, Xia *et al.* 2022):

$$\mathbf{T} = \mathbf{E} - l^2 \nabla^2 \mathbf{E} \quad (9)$$

Table 1 Roots of fifth degree shifted Legendre polynomial

$P_5^* = 252x^5 - 630x^4 + 560x^3 - 210x^2 + 30x - 1$	
x_1	0.9531
x_2	0.7692
x_3	0.5000
x_4	0.2308
x_5	0.0469

in which \mathbf{T} is the stress tensor and l is the length scale parameter. Moreover, the operator ∇^2 in general form is defined as:

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \quad (10)$$

In the case of the Bernoulli-Euler nanobeam structure the constitutive equation reduces to:

$$T_{xx} = E_{xx} - l^2 \frac{\partial^2 E_{xx}}{\partial x^2} \quad (11)$$

3.4 Numerical solution procedure

The partial differential equations appeared in the previous sections are solved using numerical method. An effective and stable numerical method is differential quadrature method (DQM) in which the derivatives of a function is approximates by weighted sum of its value in different points. By this method the differential equation is converted to a system of linear equations. The values of the weight coefficient in the relation could be obtained using several methods depending on the level of accuracy required. Therefore, first derivative of function γ could be estimated by:

$$\gamma'(\beta_i) = \sum_{j=1}^N \alpha_{ij} \gamma(\beta_j) \quad (12)$$

Table 2 Dimensionless natural frequency of cantilever beam in comparison to Ref. (Karkon 2018) results

h/L		Mode of vibration			
		1st	2nd	3rd	4th
0.01	Present	3.1301	6.2785	9.4047	12.5357
	Ref.	3.1413	6.2811	9.4176	12.5494
0.1	Present	3.0922	6.0856	8.8364	11.3298
	Ref.	3.1157	6.0907	8.8405	11.3432
0.2	Present	3.0234	5.6598	7.8251	9.6471
	Ref.	3.0453	5.6716	7.8396	9.6572

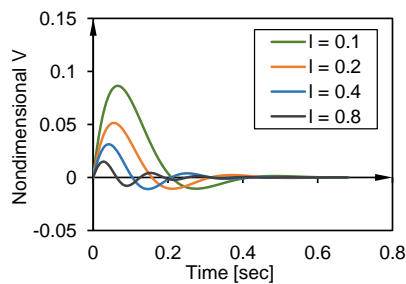


Fig. 3 Effect of length scale parameter on the produced voltage in piezoelectric layers

where, the weights are α_{ij} and N denoted number of grid points in the domain. Here, the shifted Legendre polynomial $P_n^*(x_i)$ is employed to calculate weight coefficients:

$$\alpha_{ij} = \frac{1}{\beta_i - \beta_j} \frac{P_n^*(\beta_i)}{P_n^*(\beta_j)} \quad (13)$$

In addition, roots of the Legendre polynomial are used as the grid points. The roots of fifth order Legendre polynomial is presented in Table 1.

4. Results and discussion

4.1 Validation of the numerical procedure

Numerical procedure employed in this study needs to be validated. In doing so, we solve a benchmark problem in cantilever beam without tip mass as presented by (Karkon 2018). As can be observed, the natural frequency presented by present study is lower in all h/L values and the provided mode of vibrations. One main cause of such difference is using different beam modeling. However, the results are close to each other and thereby the method of this study is validated by comparing with the reference mentioned above.

4.2 Effects of material and geometrical parameters

In this section effects of different parameters discussed in section 3 are presented. The parameters includes stiffness of the beam which is mainly controlled by CNT reinforcement weight fraction. The other parameter is the tip mass which controls the natural frequency of the beam

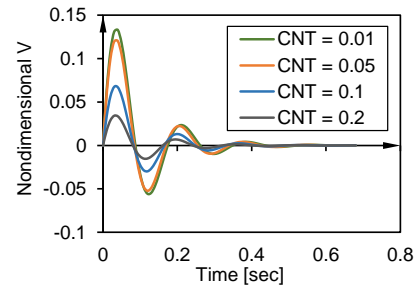


Fig. 4 Effect of CNT weight fraction on the produced voltage in piezoelectric layers

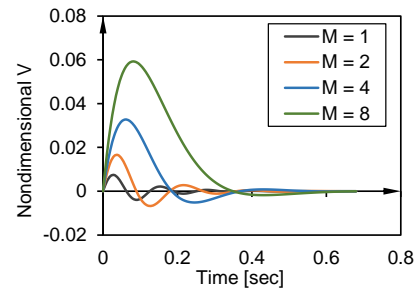


Fig. 5 Effect of nondimensional mass on the produced voltage in piezoelectric layers

in and effective way. Also, the damping characteristics of the substrate is influential to discontinue vibration of the nano-beam sensor. In addition characteristics of the piezo electric material is important in inducing voltage for infrared transmitter. To ease in reading mechanical responses the following nondimensional parameters is defined. Nondimensional height of the piezoelectric layer is the ratio of piezoelectric height h_p to the total height of the beam h or h_p/h . Nondimensional mass is defined as $\frac{M}{\rho_p A_p L}$.

In Fig. 3, effect of the length scale parameter is shown. Larger length scale parameter indicate smaller beam structure for same materials. It is seen that increasing length scale parameter cause increase in natural frequency and decrease in voltage amplitude. Both of these effects are not desirable for the purpose of this study. Therefore, smaller length parameter, i.e., larger beam, cause greater induced voltage and lower frequency and is applicable in tennis ball.

Effect of the weight fraction of CNT reinforcement is illustrated in Fig. 4. This figure shows that increasing the amount of CNT slightly increase frequency. However, it decreases the produced voltage. Thus, a compromise should be taken to have better results. One way to change this behavior is explained in the next figure.

The tip mass of the nano-beam probably has the most significant effect on the voltage amplitude and frequency as depicted in Fig. 5. Increasing mass without increase in stiffness of the structure cause larger deflection of beam and consequently induce larger voltage. In addition, larger mass reduces the frequency of vibration. It is seen in this graphs that nondimensional mass equal to 8 leads to considerably good results since large voltage and damped vibration is observed.

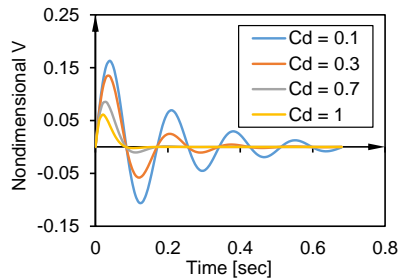


Fig 6 Effect of damping parameter of the substrate on the produced voltage in piezoelectric layers

Damping coefficient of the viscoelastic substrate reduces the voltage amplitude and increase the frequency of the vibration as shown in Fig. 6. Therefore, increase in damping has undesirable consequences in the beam structure. However, some degree of damping must exist in the beam structure to instantly reduce the voltage amplitude. If not, the infrared transmitter continues to blink and the nanosensors become useless in detecting exact moment of the impact. In this regard, it is recommended that damping coefficient be maintained at a midrange level and desired properties set with change in the tip mass.

5. Conclusions

Tracking the motion of tennis balls is a challenging task in using cameras around the tennis court. The most important instance of the tennis trajectory is the time of impact and touch the court which in some cases could not be detected precisely. In the present study, we aim to present a novel design of tennis balls equipped with nanosensors to detect the touch of the ball to the court. In the impact instance, tennis ball receives significant acceleration and change in the linear momentum. This large acceleration could deform a small-beam structure with piezoelectric layer to produce voltage. The voltage could further be utilized to produce infrared waves which could be easily detected by infrared detection sensors installed on the same video cameras or separately near the tennis court. Therefore, the exact time of the impact could be achieved with higher accuracy than image analyzing method. Detailed dynamical properties of such sensors is discussed using nonlinear beam equations. The results show that:

- Smaller length parameter, i.e., larger beam, cause greater induced voltage and lower frequency and is applicable in tennis ball.
- Nondimensional mass equal to 8 leads to considerably good results since large voltage and damped vibration is observed.
- Some degree of damping must exist in the beam structure to instantly reduce the voltage amplitude.

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