

Application of machine learning and deep neural network for wave propagation in lung cancer cell

Lumin Xing^{*1,2§}, Wenjian Liu^{2§}, Xin Li³, Han Wang⁴, Zhiming Jiang¹ and Lingling Wang^{**5}

¹The First Affiliated Hospital of Shandong First Medical University & Shandong Provincial Qianfoshan Hospital, Jinan, Shandong, 250014, China

²City University of Macau, Macau, 999078, China

³Shandong University of Political Science and Law, Jinan, Shandong, 250014, China

⁴Zhuhai Institute of Advanced Technology Chinese Academy of Sciences, Zhuhai, Guangdong, 519000, China

⁵Shandong Academy of Chinese Medicine, Jinan, 250014, Shandong, China

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Abstract. Coughing and breath shortness are common symptoms of nano (small) cell lung cancer. Smoking is main factor in causing such cancers. The cancer cells form on the soft tissues of lung. Deformation behavior and wave vibration of lung affected when cancer cells exist. Therefore, in the current work, phase velocity behavior of the small cell lung cancer as a main part of the body via an exact size-dependent theory is presented. Regarding this problem, displacement fields of small cell lung cancer are obtained using first-order shear deformation theory with five parameters. Besides, the size-dependent small cell lung cancer is modeled via nonlocal stress/strain gradient theory (NSGT). An analytical method is applied for solving the governing equations of the small cell lung cancer structure. The novelty of the current study is the consideration of the five-parameter of displacement for curved panel, and porosity as well as NSGT are employed and solved using the analytical method. For more verification, the outcomes of this reports are compared with the predictions of deep neural network (DNN) with adaptive optimization method. A thorough parametric investigation is conducted on the effect of NSGT parameters, porosity and geometry on the phase velocity behavior of the small cell lung cancer structure.

Keywords: deep neural network; nano cell lung cancer structure; NSGT; Porosity; wave propagation

1. Introduction

Nano (small) cell lung cancer (SCLC) is a prevalent cancer among smoking groups (van Meerbeek *et al.* 2011, Rudin *et al.* 2021). Indeed, smoking is a high risk factor of SCLC. The cancer cells form on the soft tissue of the lung (He *et al.* 2020, Yan *et al.* 2020, Lv *et al.* 2021, Chen *et al.* 2022b, Jin *et al.* 2022, Zhang *et al.* 2022c). Inhaling and exhaling difficulties are common symptoms of this type of disease which involves mechanical change in shape of the soft tissues and in the case of coughing vibration in the soft tissues are dominant. Since, the mechanisms of deformation in the tissues are dominantly affected by small length scale investigating deformation in the lung tissues are justifiable only using scale-capture deformation theories (Abd Wahab and Adzmi 2017, Bumidin *et al.* 2018, Wang *et al.* 2021, Zhang *et al.* 2022a, b). On the other hand, the lung structure is a porous medium. Therefore, porous elasticity methods should be used in the mechanical investigation of its behavior (Esayas and Kattimani 2021).

Wave propagation in tissue structure in coughing is a challenging problem in investigating small-cell lung cancer

(Li *et al.* 2017, Liao *et al.* 2021, Ma *et al.* 2021, Tang *et al.* 2021, Zhang *et al.* 2021a, Zheng *et al.* 2021a). Coughing in some cases causes damage to the lung tissue. The vibration and dynamical force in lung is very similar to mechanical behavior of membranes and panels. Size-dependent stress and strain gradient theories have been utilized in many investigation on nano-scale structure and functionally graded materials (Dai and Safarpour 2021, Forsat *et al.* 2021, Ghamkhar *et al.* 2021, Khadimallah *et al.* 2021a, b, Kumar *et al.* 2021, Madenci 2021, Tlidji *et al.* 2021). Oyarhossein *et al.* (2020a) utilized nonlocal stress-strain gradient theory to examine vibrational behavior of microtubule composites. Hamilton's principle in the context of small deformation of elasticity has been employed in their study. They obtained effects of different laminate orientations and nonlocal parameters on the natural frequency of the structure. Moayedi *et al.* (2021) utilized size-dependent theories to investigate buckling and vibration of cylindrical nanoshell under thermal loading. It was concluded that in length scale in the nonlocal theory had a significant influence on the natural frequencies of the structure. Zhang *et al.* (2020a) developed gradient models for beam structures base on three different beam theories. Small-scale effects were included in the vibrational analysis of beam structures using inertia gradient, strain gradient and surface energy method. Variational principle of Euler-Lagrange was employed to obtain the governing equations. They found that shape modes of the beams were substantially changed with introducing scale effects in the analysis. Vibration of doubly curved functionally graded composite was studied using strain gradient elasticity and

*Corresponding author, Ph.D.,
E-mail: xrl_net@msn.com

**Co-corresponding author, Professor,
E-mail: 870846819@qq.com

§These authors contributed equally to this work

shear defamtion theory by Karami and Shahsavari (2020). In their study, different geometries of nano-shell structure has been investigated. It was revealed that resonance in the hyperbolic geometries occurred before other investigated geometries. Sahmani *et al.* (2018) explored the vibration behavior of functionally graded porous materials using nonlocal strain gradient theory. They demonstrated that in doubly curved composite structures made from this material plate deflection and amplitude influenced behavior of the shell structure. Using classical plate theory and nonlocal strain gradient constitutive equations (Habibi *et al.* 2016, 2018a, b, 2019b, d, e Ebrahimi *et al.* 2019a, Esmailpoor Hajilak *et al.* 2019, Pourjabari *et al.* 2019, Safarpour *et al.* 2019a), Ebrahimi and Dabbagh (2020) computed frequencies of a composite plate using analytical solutions. A detailed parameter study was further conducted to observe most important parameters affecting vibration of the plate. Responses of nano-scale rotating circular plate made of FG material were presented by Mahinzare *et al.* (2019) employing nonlocal Eringen formulation, nonlocal and classic strain gradient theory and of plate structure. Effects of different parameters were examined on the vibrational behavior of the plate. There many reports on the using of nonlocal stress and strain gradient theories on the static and dynamic behavior of the structures (Al-shujairi and Mollamahmutoğlu 2018, Karami and Shahsavari 2019, lori *et al.* 2020b, Huang *et al.* 2021a, Zhang *et al.* 2021b).

Porosity in materials cause different responses of bio and structural material under thermal, static and dynamic loadings (Safarpour *et al.* 2018, 2019b, 2020, Habibi *et al.* 2017, 2019a, c, Alipour *et al.* 2020, Ebrahimi *et al.* 2020a, Ghazanfari *et al.* 2020, Chen *et al.* 2022a). In this regard, Lande and Mitzner (2006) modeled air flow in the lung considering the lung materials as viscoelastic material to observe dynamical responses in bith healthy and diseased lungs. Kowalczyk (1993) used nonlinear elasticity and perfect air equations to model solid and gaseous parts of the two-phase solid/air lung. The constitutive equations of the two phase material were developed and matrix form was presented for further finite element analysis. Ramteke and Panda (2021) examined effect of porosity on the free vibration of graded structure. They considered different pattern of porosity distribution. It was revealed that porosity pattern could alter the vibrational behavior significantly. The mechanical properties of porous medium are averaged and a continuum model is used to analyze the static and dynamical behavior of the structures (Massoumi *et al.* 2018). Seyfi *et al.* (2016) compared computational and actual deformation of lung during breathing engaging a poro-elastic model. The lung geometry was constructed using high-resolution images and fluid-solid interaction finite element method employed to find the deformation of the lung. There are several studies on the mechanical behavior of lung during breathing (Fredberg and Stamenovic 1989, Ilegbusi *et al.* 2015, Seyfi Noferest *et al.* 2015). However, small-scale effects in lung have not been properly addressed. Karimiasl *et al.* (2019) employed size-dependent elasticity theories to procure vibration and buckling responses of porous structure with fluid flow. Analytical solutions were presented and the results revealed that fluid flow inside the porous medium substantially alter vibrational behavior of the structure. Gao *et al.* (2020) investigated wave propagation in functionally graded

porous medium and considered various porosity patterns in their analysis. They concluded that the wave propagation in porous medium is highly reliant on the porosity distribution.

Marchesseau *et al.* (2010) presented a nonlinear viscoelastic model for porous material with the focus on the human organs. They provide application of the model in surgery of liver. A porohyperviscoelastic model (Zheng *et al.* 2021b) to investigate effect of internal pressure on the shear wave motion in soft tissues similar to liver. Mechanics of soft tissues are investigated in other references to examine wave propagation in the human organs (Sevostianov and Kachanov 2000, Evans *et al.* 2013, MacMinn *et al.* 2016)

For the first time, phase velocity analysis of a small cell lung cancer structure employing first-order shear deformation theory is presented. The current small cell lung cancer structure is modeled using curved panel system with porosity. Besides, the size-dependent small cell lung cancer structure is simulated via NSGT. A detailed analytical procedure is utilized for solving the governing equations of the small cell lung cancer structure. For more verification, the outcomes of the present reports are compared with the predictions of adaptively tuned DNN. A thorough parametric investigation is conducted on the effect of NSGT parameter, porosity level and geometry on the phase velocity response of the small cell lung cancer structure.

2. Governing equations

Displacement components in a curves shell structure in the FSDT is regarded as (Wang *et al.* 2018, Karami and Shahsavari 2020):

$$\begin{aligned} u(x, y, h, t) &= u_0(x, y, t) + hu_1(x, y, t) \\ v(x, y, h, t) &= v_0(x, y, t) + hv_1(x, y, t) \\ w(x, y, h, t) &= w_0(x, y, t) \end{aligned} \quad (1a)$$

in which u_0 , v_0 , and w_0 show, respectively, the mid-plane displacements along the x , y , and z directions. The terms u_1 and v_1 are shear rotations functions. In addition, the non-zero components of normal and shear strains can be obtained as given below (Wang *et al.* 2018, Karami and Shahsavari 2020):

$$\begin{Bmatrix} \varepsilon_{xx} \\ \varepsilon_{yy} \\ \gamma_{\gamma y} \\ \gamma_{\gamma h} \\ \gamma_{yh} \end{Bmatrix} = \begin{Bmatrix} \frac{\partial u_0}{\partial x} + z \frac{\partial u_1}{\partial x} + \frac{w_0}{R_y} \\ \frac{\partial v_0}{\partial y} + h \frac{\partial v_1}{\partial y} \\ \frac{\partial u_0}{\partial y} + h \frac{\partial u_1}{\partial y} + \frac{\partial v_0}{\partial x} + z \frac{\partial v_1}{\partial x} \\ u_1 + \frac{\partial w_0}{\partial x} - \frac{1}{R_y}(u_0) \\ v_1 + \frac{\partial w_0}{\partial y} \end{Bmatrix} \quad (1b)$$

Material properties are functions of position and well as porosity level in porous materials (Mohammadhassani *et al.* 2013, 2014, Toghrolri *et al.* 2014, 2016, Safa *et al.* 2016, 2020b, Sadeghipour Chahnasir *et al.* 2018, Sedghi *et al.* 2018, Katebi *et al.* 2019, Shariati *et al.* 2019b, 2020n, o, p, q, 2021d). The following relations is adopted for the module of elasticity, density and Poisson's ratio (Sahmani

et al. 2018):

$$\begin{aligned} E_p &= E[1 - \alpha_p \beta(z)], \\ \rho_p &= \rho[1 - \alpha_m \beta(z)], \\ v_p &= 0.221 \left(1 - \frac{\rho_p}{\rho}\right) \\ &+ v \left[1 + 0.342 \left(1 - \frac{\rho_p}{\rho}\right)^2 - 1.21 \left(1 - \frac{\rho_p}{\rho}\right)\right] \end{aligned} \quad (2)$$

where

$$\begin{aligned} \beta(z) &= \begin{cases} \cos\left(\frac{\pi z}{2h} + \frac{\pi}{4}\right) \text{imperfection1} \\ \cos\left(\frac{\pi z}{h}\right) \text{imperfection2} \end{cases} \\ \alpha_m &= \frac{1.121}{\beta(z)} \left\{1 - [1 - \alpha_p \beta(z)]^{\frac{1}{2.3}}\right\} \end{aligned} \quad (3)$$

The constants α_m and α_p in Eqs. (2) and (3) are density and porosity factors, respectively. Moreover, E_p , v_p and ρ_p are isotropic module of elasticity, Poisson’s ratio and density of the porous material, respectively. The linear constitutive equations of the porous material can be given as (Ebrahimi et al. 2019b, c, 2020b, Hashemi et al. 2019, Moayedi et al. 2019, 2020a, b, Mohammadgholiha et al. 2019, Mohammadi et al. 2019, Habibi et al. 2020, Oyarhossein et al. 2020b, Shariati et al. 2020h, k, Shokrgozar et al. 2020):

$$\begin{bmatrix} \sigma_{xx} \\ \sigma_{yy} \\ \sigma_{xy} \\ \sigma_{xh} \\ \sigma_{yh} \end{bmatrix} = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & 0 & 0 & 0 \\ \bar{Q}_{21} & \bar{Q}_{22} & 0 & 0 & 0 \\ 0 & 0 & \bar{Q}_{44} & 0 & 0 \\ 0 & 0 & 0 & \bar{Q}_{55} & 0 \\ 0 & 0 & 0 & 0 & \bar{Q}_{66} \end{bmatrix} \begin{bmatrix} \varepsilon_{xx} \\ \varepsilon_{yy} \\ \varepsilon_{xy} \\ \varepsilon_{xh} \\ \varepsilon_{yh} \end{bmatrix} \quad (4a)$$

The terms used in Eq. (4a) would be obtained as (Mohammadreza 2012, Aghakhani et al. 2015, Toghroli 2015, 2018, 2020, Mohammadhassani et al. 2015, Sari et al. 2019, Xu et al. 2019, Jermisittiparsert et al. 2020, Safa et al. 2020a, Shariati et al. 2014, 2020a, b, c, d, e, f, g, j, i, m, 2021a, b, c.):

$$\begin{aligned} \bar{Q}_{11} &= \frac{E_{11}}{1 - \nu_{12}\nu_{21}}, \bar{Q}_{12} = \frac{\nu_{12}E_{22}}{1 - \nu_{12}\nu_{21}}, \\ \bar{Q}_{22} &= \frac{E_{22}}{1 - \nu_{12}\nu_{21}}, \bar{Q}_{44} = G_{12}, \bar{Q}_{55} = G_{23}, \bar{Q}_{66} = G_{13}. \end{aligned} \quad (4b)$$

Also, the strains relations are (Liu et al. 2020b, 2021b, Habibi et al. 2021, He et al. 2021, Huang et al. 2021a, Zhang et al. 2021):

2.1 Hamilton’s principle and its extended form

Energy equations of the structure are obtained using the well-known Hamilton’s principle (Hashemi et al. 2019, Al-Furjan et al. 2020c, d, e, f, Bai et al. 2020, Cheshmeh et al. 2020, Li et al. 2020a, Lori et al. 2020a, Najaafi et al. 2020, Shariati et al. 2020l, Zhang et al. 2020b, Guo et al. 2021b, Liu et al. 2021a). In the current study, the extended from of this principle is utilized in the following relations:

$$\int_{t_1}^{t_2} (\delta \Pi_u - \delta \Pi_k) dt = 0 \quad (5)$$

The components of the first strain energy (Adamian et al. 2020, Al-Furjan et al. 2020a, b, Li et al. 2020b, Liu et al.

2020b, Zare et al. 2020, Dai et al. 2021b, Habibi et al. 2021, He et al. 2021, Huang et al. 2021b, Liu et al. 2021b, Zhang et al. 2021b) term is calculated using Eq. (1) as given below:

$$\begin{aligned} \delta \Pi_u &= \iiint_V \sigma_{ij} \delta \varepsilon_{ij} dV = \\ &= \iint_A \left[\begin{aligned} &N_{\gamma\gamma} \left(\frac{\partial \delta u_0}{\partial \gamma} + \frac{\delta w_0}{R_\gamma} \right) + M_{\gamma\gamma} \frac{\partial \delta u_1}{\partial \gamma} \\ &+ N_{yy} \left(\frac{\partial \delta v_0}{\partial y} \right) + M_{yy} \frac{\partial \delta v_1}{\partial y} \\ &+ N_{yz} \left(\delta v_1 + \frac{\partial \delta w_0}{\partial y} \right) \\ &+ N_{yz} \left(\delta u_1 + \frac{\partial \delta w_0}{\partial \gamma} - \frac{\delta u_0}{R_\gamma} \right) + M_{yz} \left(-\frac{\delta u_1}{R_\gamma} \right) \\ &+ N_{\gamma\gamma} \left(\frac{\partial \delta u_0}{\partial y} + \frac{\partial \delta v_0}{\partial \gamma} \right) + M_{\gamma\gamma} \left(\frac{\partial \delta u_1}{\partial y} + \frac{\partial \delta v_1}{\partial \gamma} \right) \end{aligned} \right] dA \end{aligned} \quad (6a)$$

where

$$\{N_{ij}, M_{ij}\} = \int_z \{\sigma_{ij}, z\sigma_{ij}\} dz \quad (6b)$$

In addition, the kinetic energy (Liu et al. 2020a, Wang et al. 2020, Zhou et al. 2020, Dai et al. 2021a, Guo et al. 2021a, Shao et al. 2021, Wu and Habibi 2021) term can be calculated using the following:

$$\delta \Pi_k = \int_z \iint_A \rho \left\{ \frac{\partial u}{\partial t} \frac{\partial \delta u}{\partial t} + \frac{\partial v}{\partial t} \frac{\partial \delta v}{\partial t} + \frac{\partial w}{\partial t} \frac{\partial \delta w}{\partial t} \right\} dA \quad (7)$$

As a consequent, substituting Eqs. (8), (7), and (6a) in Eq. (5), equations of motion of the porous doubly-curved shell are achieved as given below for different directions:

$$\begin{aligned} \delta u_0: & \frac{\partial N_{\gamma\gamma}}{\partial \gamma} + \frac{\partial N_{yy}}{\partial y} + \frac{N_{\alpha\gamma}}{R_\gamma} = I_0 \frac{\partial^2 u_0}{\partial t^2} + I_1 \frac{\partial^2 u_1}{\partial t^2}, \\ \delta v_0: & \frac{\partial N_{yy}}{\partial y} + \frac{\partial N_{yz}}{\partial \gamma} = I_0 \frac{\partial^2 v_0}{\partial t^2} + I_1 \frac{\partial^2 v_1}{\partial t^2}, \\ \delta w_0: & \frac{\partial N_{yz}}{\partial y} + \frac{\partial N_{yz}}{\partial \gamma} - \frac{N_{\gamma\gamma}}{R_\gamma} = I_0 \frac{\partial^2 w_0}{\partial t^2}, \\ \delta u_1: & \frac{\partial M_{\gamma\gamma}}{\partial \gamma} + \frac{\partial M_{yy}}{\partial y} + \frac{M_{yz}}{R_\gamma} - N_{yz} = I_1 \frac{\partial^2 u_0}{\partial t^2} + I_2 \frac{\partial^2 u_1}{\partial t^2}, \\ \delta v_1: & \frac{\partial M_{yy}}{\partial y} + \frac{\partial M_{\gamma\gamma}}{\partial \gamma} - N_{yz} = I_1 \frac{\partial^2 v_0}{\partial t^2} + I_2 \frac{\partial^2 v_1}{\partial t^2}. \end{aligned} \quad (8)$$

where

$$\{I_i\} = \int_{-\frac{h}{2}}^{\frac{h}{2}} \rho \{z^i\} dz \quad (9)$$

2.2 Applying size-dependent theory

In the nonlocal strain gradient theory, both nonlocal stresses and strain gradient are considered in the constitutive equations of the material (Arabnejad Khanouki et al. 2010, Mojtaba 2011, Shariati et al. 2011a, b, 2019a, c, d, e, 2020r, Sinaei et al. 2011, 2012, Mansouri et al. 2016, Shahabi et al. 2016, Khorramian et al. 2017, Nosrati et al. 2018, Ziaei-Nia et al. 2018, Milovancevic et al. 2019, Sajedi and Shariati 2019, Trung et al. 2019a, b, Afshar et al. 2020, Yazdani et al. 2020, Davoodnabi et al. 2021). Therefore,

the relationship between stress and strain in this theory includes both gradients of stress and strain fields:

$$(\mathbf{1} - \nabla^2 \mu^2) \sigma_{ij} = (\mathbf{1} - \nabla^2 l^2) \mathbf{Q}_{ij} \varepsilon_{ij} \quad (10)$$

In Eq. (9), ∇^2 represent the Laplacian operator. Substituting Eqs. (10), and (4a) in Eq. (8) the equations of motion for the current small cell lung cancer structure can be obtained as given below:

$$\begin{aligned} \delta u_0: (1 - \nabla^2 l^2) & \left(\begin{array}{l} \frac{\partial}{\partial y} \left(\begin{array}{l} A_{11} \frac{\partial u_0}{\partial y} + B_{11} \frac{\partial u_1}{\partial y} \\ + A_{11} \frac{w_0}{R_y} + A_{12} \frac{\partial v_0}{\partial y} + B_{12} \frac{\partial v_1}{\partial y} \end{array} \right) \\ + \frac{\partial}{\partial y} \left(\begin{array}{l} A_{44} \frac{\partial u_0}{\partial y} + B_{44} \frac{\partial u_1}{\partial y} \\ + A_{44} \frac{\partial v_0}{\partial y} + B_{44} \frac{\partial v_1}{\partial y} \end{array} \right) \\ + \frac{1}{R_y} \left(\begin{array}{l} A_{55} u_1 + A_{55} \frac{\partial w_0}{\partial y} \\ - \frac{1}{R_y} (A_{55} u_0 + B_{55} u_1) \end{array} \right) \end{array} \right) \\ = (1 - \nabla^2 \mu^2) & \left(I_0 \frac{\partial^2 u_0}{\partial t^2} + I_1 \frac{\partial^2 u_1}{\partial t^2} \right) \end{aligned} \quad (11a)$$

$$\begin{aligned} \delta v_0: (1 - \nabla^2 l^2) & \left(\begin{array}{l} \frac{\partial}{\partial y} \left(\begin{array}{l} A_{21} \frac{\partial u_0}{\partial y} + B_{21} \frac{\partial u_1}{\partial y} \\ + A_{21} \frac{w_0}{R_y} + A_{11} \frac{\partial v_0}{\partial y} + B_{11} \frac{\partial v_1}{\partial y} \end{array} \right) \\ + \frac{\partial}{\partial y} \left(\begin{array}{l} A_{44} \frac{\partial u_0}{\partial y} + B_{44} \frac{\partial u_1}{\partial y} \\ + A_{44} \frac{\partial v_0}{\partial y} + B_{44} \frac{\partial v_1}{\partial y} \end{array} \right) \end{array} \right) \\ = (1 - \nabla^2 \mu^2) & \left(I_0 \frac{\partial^2 v_0}{\partial t^2} + I_1 \frac{\partial^2 v_1}{\partial t^2} \right) \end{aligned} \quad (11b)$$

$$\begin{aligned} \delta w_0: (1 - \nabla^2 l^2) & \left(\begin{array}{l} \frac{\partial}{\partial y} \left(A_{66} v_1 + A_{66} \frac{\partial w_0}{\partial y} \right) \\ + \frac{\partial}{\partial y} \left(\begin{array}{l} A_{55} u_1 + A_{55} \frac{\partial w_0}{\partial y} \\ - \frac{1}{R_y} (A_{55} u_0 + B_{55} u_1) \end{array} \right) \\ - \frac{1}{R_y} \left(\begin{array}{l} A_{11} \frac{\partial u_0}{\partial y} + B_{11} \frac{\partial u_1}{\partial y} \\ + A_{11} \frac{w_0}{R_y} + A_{12} \frac{\partial v_0}{\partial y} + B_{12} \frac{\partial v_1}{\partial y} \end{array} \right) \end{array} \right) \\ = (1 - \nabla^2 \mu^2) & \left(I_0 \frac{\partial^2 w_0}{\partial t^2} \right) \end{aligned} \quad (11c)$$

$$\begin{aligned} \delta u_1: (1 - \nabla^2 l^2) & \left(\begin{array}{l} \frac{\partial}{\partial y} \left(\begin{array}{l} B_{11} \frac{\partial u_0}{\partial y} + C_{11} \frac{\partial u_1}{\partial y} \\ + B_{11} \frac{w_0}{R_y} + B_{12} \frac{\partial v_0}{\partial y} + C_{12} \frac{\partial v_1}{\partial y} \end{array} \right) \\ + \frac{\partial}{\partial y} \left(\begin{array}{l} B_{44} \frac{\partial u_0}{\partial y} + C_{44} \frac{\partial u_1}{\partial y} \\ + B_{44} \frac{\partial v_0}{\partial y} + C_{44} \frac{\partial v_1}{\partial y} \end{array} \right) \\ + \frac{1}{R_y} \left(\begin{array}{l} B_{55} u_1 + B_{55} \frac{\partial w_0}{\partial y} \\ - \frac{1}{R_y} (B_{55} u_0 + C_{55} u_1) \end{array} \right) \\ - \left(\begin{array}{l} A_{55} u_1 + A_{55} \frac{\partial w_0}{\partial y} \\ - \frac{1}{R_y} (A_{55} u_0 + B_{55} u_1) \end{array} \right) \end{array} \right) \end{aligned} \quad (11d)$$

$$\begin{aligned} & = (1 - \nabla^2 \mu^2) \left(I_1 \frac{\partial^2 u_0}{\partial t^2} + I_2 \frac{\partial^2 u_1}{\partial t^2} \right) \\ & \left(\begin{array}{l} \frac{\partial}{\partial y} \left(\begin{array}{l} B_{21} \frac{\partial u_0}{\partial y} + C_{21} \frac{\partial u_1}{\partial y} \\ + B_{21} \frac{w_0}{R_y} + B_{11} \frac{\partial v_0}{\partial y} + C_{11} \frac{\partial v_1}{\partial y} \end{array} \right) \\ + \frac{\partial}{\partial y} \left(\begin{array}{l} B_{44} \frac{\partial u_0}{\partial y} + C_{44} \frac{\partial u_1}{\partial y} \\ + B_{44} \frac{\partial v_0}{\partial y} + C_{44} \frac{\partial v_1}{\partial y} \end{array} \right) \\ - \left(A_{66} v_1 + A_{66} \frac{\partial w_0}{\partial y} \right) \end{array} \right) \\ & = (1 - \nabla^2 l^2) \left(I_1 \frac{\partial^2 v_0}{\partial t^2} + I_2 \frac{\partial^2 v_1}{\partial t^2} \right) \end{aligned} \quad (11e)$$

where

$$\{A_{ij}, B_{ij}, C_{ij}\} = \{1, z, z^2\} \sigma_{ij} dz \quad (12)$$

3. Solution method

A harmonic field of displacement as complex exponential function is assumed as follows (Ma *et al.* 2022, Zhao *et al.* 2022, Habibi *et al.* 2019d, Hou *et al.* 2021, Huang *et al.* 2021c, d, Jiao *et al.* 2021, Liu *et al.* 2021c, Moradi *et al.* 2021, Xu *et al.* 2021, Dong *et al.* 2022, Luo *et al.* 2022, Yang *et al.* 2022, Yu *et al.* 2022):

$$\begin{Bmatrix} u_0 \\ v_0 \\ w_0 \\ u_1 \\ v_1 \end{Bmatrix} = \begin{Bmatrix} U_0 \exp(m\gamma + ny - \omega t)i \\ V_0 \exp(m\gamma + ny - \omega t)i \\ W_0 \exp(m\gamma + ny - \omega t)i \\ U_1 \exp(m\gamma + ny - \omega t)i \\ V_1 \exp(m\gamma + ny - \omega t)i \end{Bmatrix} \quad (13)$$

in which wave numbers along axial and circumferential directions are represented by m and n , respectively. In addition, ω is the frequency of vibration of the structure. Replacing Eq. (13) into equations of motion without considering damping effects results in:

$$(\omega^2 [M] - [K]) \{d\} = \{0\} \quad (14)$$

where

$$\{d\} = \{u_0 \quad v_0 \quad w_0 \quad u_1 \quad v_1\} \quad (15)$$

Moreover, the phase velocity is considered to have the following:

$$S = \frac{\omega}{n} \quad (16)$$

4. Comparative study using deep learning model

Deep learning and machine learning models have been commonly used in the field of regression. These methods, in general, utilized a set of input data to learn the behavior of the system and later uses the trained model for further predictions. Therefore, having enough data to train the model, these network could be utilize for prediction of behavior of the small cell lung cancer vibrations.

The learning procedure is simple and straight forward. A deep neural network (DNN) initiates its prediction with arbitrary constants for regression functions also known as weight and biases. Then, the outcome of the network compared with the actual outcome provided in data set. If the differences between predicted and actual outputs are not desirable, the network utilized an optimization algorithm to adjust regression constants until the desire values obtained by network. At the end, the network is tested to find out the accuracy of the DNN in predicting unknown problems.

In the current study, the inputs of the DNN network is vector $X = \{a/h, l, \mu, R/h, \alpha_p\}^T$ and its output is phase velocity. The optimization method is called ADADELTA (adaptive delta) method in which the mean squared error between predicted values and actual data is minimized (Yegnanarayana 2009):

$$MSE = \frac{1}{n} \sum_{i=1}^n (Y - \hat{Y})^2 \tag{17}$$

4.1 ADADELTA optimization to adjust the DNN parameters

ADADELTA optimization method is a reliable and fast algorithm in the neural network which the learning rate can be adjusted automatically. In addition, this method is not affected by the hyperparameters of the network. On the other hand, both distributed and local factors are involved in this method. The optimization procedure, tuning the weights and biases of the network, at each iteration uses the following returning equations:

$$\begin{aligned} \chi_{t+1} &= \chi_t + \Delta \chi_t \\ \Delta \chi_t &= -\eta \frac{\partial f(\chi_t)}{\partial \chi_t} \end{aligned} \tag{18}$$

where the initial learning rate is represented by parameter η . In the next steps the notation G_t will be used instead of $\frac{\partial f(\chi_t)}{\partial \chi_t}$. The root mean square gradient of the following function should be calculated at each iteration (epoch) to optimally adjust the constants of the DNN network:

$$RMS[G_t] = \sqrt{E[G_t^2] + \varepsilon} \tag{19}$$

where, ε is a constant. It should be noted that $E[G_t^2]$ represents the expected value of the square of gradient which can be determined using the given relation below:

$$E[G_t^2] = \rho E[G_{t-1}^2] + (1 - \rho)G_t^2 \tag{20}$$

where, ρ denotes the decay rate. Utilizing Eq. (19) and Eq. (20), the following equation could be given for updating network parameters:

$$\Delta \chi_t = -\frac{\eta}{RMS[G_t]} G_t \tag{21}$$

The ADADELTA optimization is a high performance optimizing procedure as shown by Zeiler (2012) among all other optimization method which gives the minimized error in reduced steps.

Table1 Comparison of the dimensionless natural frequency $(\omega h \sqrt{\frac{\rho}{E}})$ of simply-supported square perfect panel ($a/h=5$)

E_1/E_2	Ref. (Noor 1973)	Ref. (Khdeir 1988)	Current study
10	0.32841	0.33095	0.33108
20	0.38241	0.38110	0.38123
30	0.41089	0.41094	0.41099
40	0.43006	0.43155	0.43161

5. Results

Used parameters:

μ/h	Dimensionless nonlocal parameter
l/h	Dimensionless length scale parameter
n	Circumferential wave number
m	Axial wave number
R_γ	Radius curvature
a	Length of the structure
h	Thickness of the structure
α_p	Porosity coefficient

The proposed model for exploring vibration of porous medium is scrutinized to discover the validity of the results. In this regard, dimensionless natural frequency as calculated by the presented model is compared to the previously measured natural frequencies in the literature (Noor 1973, Khdeir 1988). The results are given in 0. As seen, there is a minor difference between the method of the current study and other methods in literature affirming the viability of the model.

The trained deep neural network performance is explained in this section. For this aim, different geometrical condition of the structure is presented in 0 and 0. As can be observed, the mean square error of the training process is very low and in lower MSE, values given by the DNN are approaching the values of numerical study in all geometrical conditions. In 0, effect of the dimensionless length scale parameters l/h is presented for different values of dimensionless nonlocal parameter μ/h . The accuracy of the DNN model is evident in the data in this table with the maximum error 1% for the case of $MSE_{Train} = 0.41 \times 10^{-6}$.

The effect of dimensionless radius of the shell structure is given in 0. Similar accuracy is observed in this table. Therefore, it can be concluded that DNN model is reliable for different geometrical condition taking the value of training mean squared error as low as possible.

The material properties of the current biological structure can be used in Ref. in detail. In this section influence of different geometrical parameters on the natural

Table 2 Prediction on the performance of DNN model toward test data (phase velocity (10^2)) for various sigma and MSN parameters for various dimensionless nonlocal and length scale parameters

$l/h=0$				
Predicted				
	Fit	$MSE_{Train} = 0.21 \times 10^{-6}$	$MSE_{Train} = 0.31 \times 10^{-6}$	$MSE_{Train} = 0.41 \times 10^{-6}$
$\mu/h=0$	0.4535	0.415698	0.436598	0.452352
$\mu/h=0.1$	0.4236	0.385469	0.405659	0.421236
$\mu/h=0.2$	0.4126	0.354566	0.384569	0.411025
$\mu/h=0.3$	0.3956	0.336598	0.369852	0.391256
$\mu/h=0.4$	0.3899	0.295698	0.356598	0.388805
$l/h=0.1$				
$\mu/h=0$	0.4605	0.425469	0.445659	0.461235
$\mu/h=0.1$	0.4245	0.395698	0.415236	0.425659
$\mu/h=0.2$	0.4149	0.369856	0.398569	0.415987
$\mu/h=0.3$	0.3921	0.345698	0.378965	0.391569
$\mu/h=0.4$	0.3978	0.305236	0.359856	0.398565
$l/h=0.2$				
$\mu/h=0$	0.4645	0.429658	0.449659	0.465659
$\mu/h=0.1$	0.4289	0.399569	0.419659	0.429658
$\mu/h=0.2$	0.4163	0.375659	0.400123	0.419658
$\mu/h=0.3$	0.3933	0.350010	0.381089	0.394655
$\mu/h=0.4$	0.3999	0.309856	0.362365	0.400012

Table 3 Prediction on the performance of DNN model toward test data (phase velocity (10^2)) for various sigma and MSN parameters for various R/h , and a/h

$R_\gamma/h=0.8$				
Predicted				
	Fit	$MSE_{Train} = 0.21 \times 10^{-6}$	$MSE_{Train} = 0.31 \times 10^{-6}$	$MSE_{Train} = 0.41 \times 10^{-6}$
$\mu/h=0$	0.4535	0.415698	0.436598	0.452352
$\mu/h=0.1$	0.4236	0.385469	0.405659	0.421236
$\mu/h=0.2$	0.4126	0.354566	0.384569	0.411025
$\mu/h=0.3$	0.3956	0.336598	0.369852	0.391256
$\mu/h=0.4$	0.3899	0.295698	0.356598	0.388805
$R_\gamma/h=0.9$				
$a/h=0.06$	0.4120	0.365469	0.385659	0.418235
$a/h=0.08$	0.3985	0.356698	0.375236	0.399659
$a/h=0.1$	0.3790	0.332856	0.359569	0.385987
$a/h=0.12$	0.3750	0.301698	0.368965	0.381569
$a/h=0.14$	0.3685	0.300236	0.331856	0.369565
$R_\gamma/h=1$				
$a/h=0.06$	0.4256	0.372658	0.401659	0.428659
$a/h=0.08$	0.4010	0.365569	0.389659	0.409658
$a/h=0.1$	0.3985	0.341659	0.365123	0.399658
$a/h=0.12$	0.3859	0.311010	0.371089	0.388655
$a/h=0.14$	0.3789	0.310856	0.340365	0.385012

frequency of the structure are presented. In 0, effect of the dimensionless length scale parameter l/h on the natural frequency is given for various values of parameter a/h .

Increasing parameter l/h cause slight increase in natural frequency of the shell structure. On the other hand, increasing a/h significantly decreases the natural frequency

Table 4 Effect of geometrical parameters dimensionless $\frac{l}{h}$ and $\frac{a}{h}$ on the natural frequency of the structure

	$l/h=0$	$l/h=0.1$	$l/h=0.2$	$l/h=0.3$
$a/h=0.08$	345.659	351.569	353.659	356.985
$a/h=0.1$	333.659	339.658	342.659	346.658
$a/h=0.12$	310.659	313.365	316.598	318.266

Table 5 Effect of geometrical parameters dimensionless $\frac{\mu}{h}$ and $\frac{a}{h}$ on the natural frequency of the structure

	$l/h=0$	$l/h=0.1$	$l/h=0.2$	$l/h=0.3$
$a/h=0.08$	343.859	341.985	339.569	335.598
$a/h=0.1$	341.759	339.658	337.585	332.569
$a/h=0.12$	307.659	306.569	304.658	302.159

Table 6 Impact of curvature of the shell structure on the natural frequency for various values of $\frac{a}{h}$

	$l/h=0$	$l/h=0.1$	$l/h=0.2$	$l/h=0.3$
$a/h=0.08$	$R_v/h=0.8$	$R_v/h=0.9$	$R_v/h=1$	$R_v/h=1.1$
$a/h=0.1$	342.985	343.105	343.569	343.896
$a/h=0.12$	340.659	341.215	341.856	342.105

for all values of dimensionless length scale parameter. Therefore, increase in length scale parameter is in favor of vibrational behavior of the structure.

In 0, effect of the dimensionless nonlocal parameter μ/h on the natural frequency is given for various values of parameter a/h . Increasing parameter μ/h cause slight decrease in natural frequency of the shell structure. In addition, increasing a/h reduces the natural frequency for all values of dimensionless nonlocal parameter. Therefore, increase in nonlocal parameter cause deterioration in frequency response of the structure.

Radius of curvature also impacts the natural frequency. Increasing the curvature cause insignificant reduction in natural frequency for all values of a/h as given in 0. Thus, curvature of the shell structure is not an important parameter in determining natural frequency of the structure and in design of such structure focus should be on the ratio of a/h , nonlocal and length scale parameters.

Influences of different parameters on the phase velocity are clarified in this section. Phase velocity is a function of nonlocal parameter as shown in Fig. 1. The effect of increasing nonlocal parameter on the phase velocity is highly dependent on the axial wave number m . In low wave numbers increasing nonlocal parameters cause a minor decrease in the phase velocity. For higher values of the axial wave number, the decrease in the phase velocity is significant in which at $m = 400$ phase velocity reduces from $6000m/s$ to $2000m/s$ by increasing dimensionless nonlocal parameter from 0 to 4. Influence of increasing axial wave number is more pronounced at lower nonlocal parameter.

In Fig. 2, the similar effects is seen effect of increasing nonlocal parameter on the phase velocity is highly

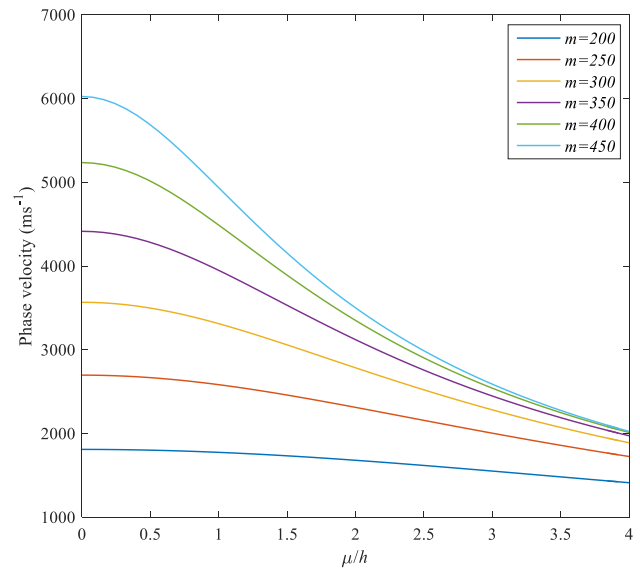


Fig. 1 Phase velocity of the structure for different values of axial wave number m as function of dimensionless nonlocal parameter

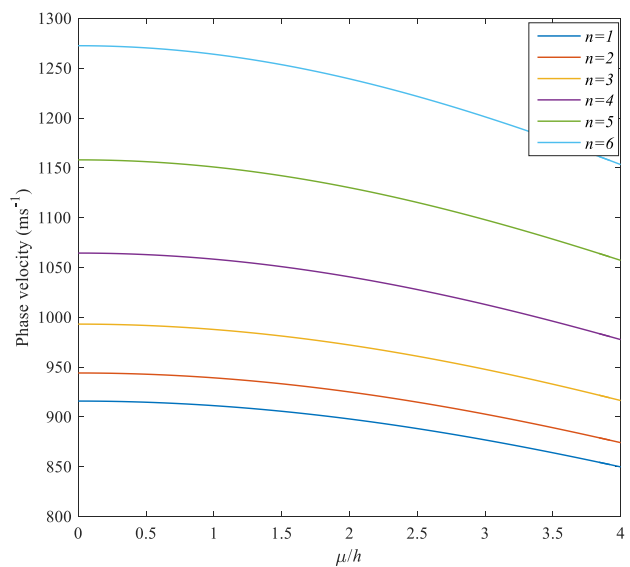


Fig. 2 Phase velocity of the structure for different values of circumferential wave number n as function of dimensionless nonlocal parameter

dependent on the circumferential wave number n . In all circumferential wave numbers, phase velocity decreases virtually at same ratio with increasing dimensionless nonlocal parameters from 0 to 4. Moreover, increase in wave number results in rise in the phase velocity.

Geometrical parameters in h/a also changes the phase velocity as depicted in Fig. 3. With increase in h/a parameter, phase velocity receive considerable growth from $750m/s$ to $1630m/s$. On the other hand, at higher values of the h/a or when the shell thickness become thinner, the behavior of the phase velocity function changes so that its curve versus nonlocal parameter has more descending gradient than curves associated with lower value of h/a .

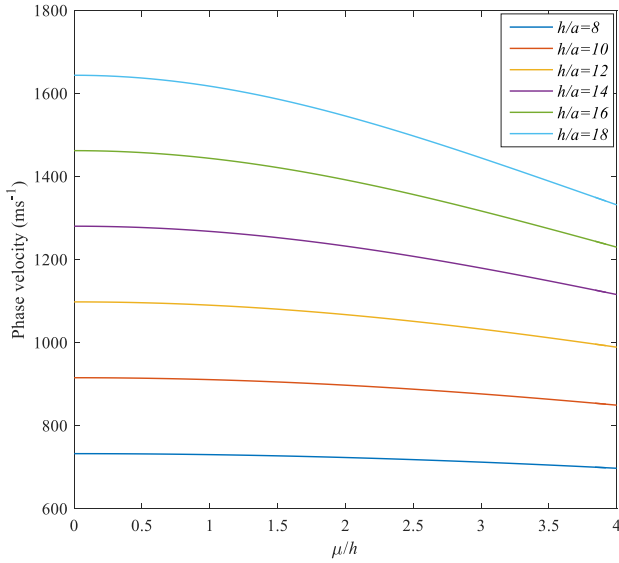


Fig. 3 Phase velocity of the structure for different values of geometrical parameter h/a as function of dimensionless nonlocal parameter

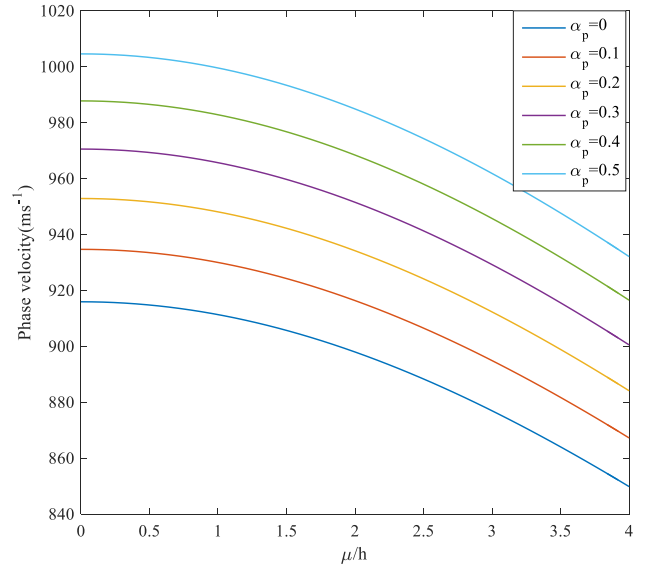


Fig. 5 Phase velocity of the structure for different values of porosity coefficient α_p as function of dimensionless nonlocal parameter

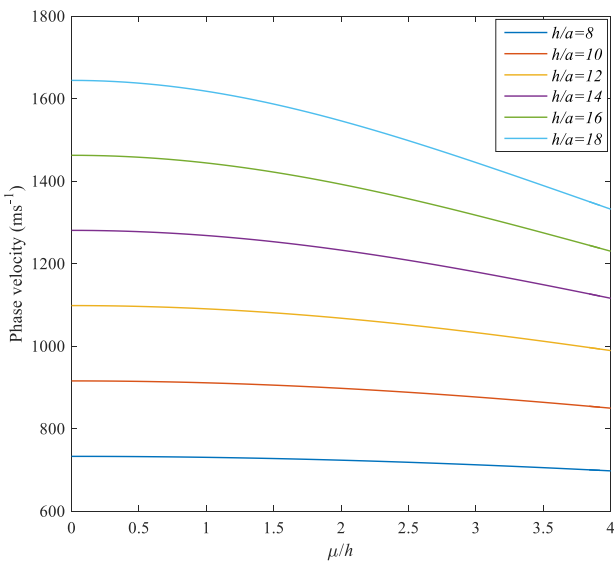


Fig. 4 Phase velocity of the structure for different values of circumferential wave number n as function of dimensionless nonlocal parameter

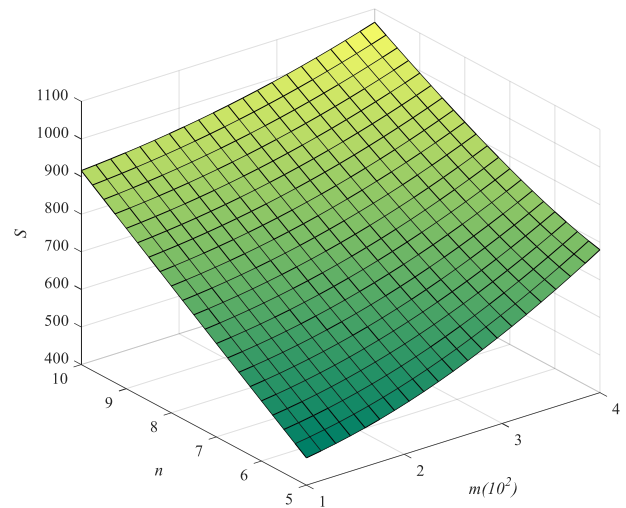


Fig. 6 Phase velocity of the structure for different values of circumferential wave number n as function of dimensionless nonlocal parameter

Porosity existence in general increase the phase velocity of the shell structure as depicted in Fig. 5. It is clear from this figure that increase in porosity of the structure does change the behavior of the phase velocity function. However, it increases the phase velocity at a constant rate. It means, independent from the value of nonlocal parameter, increasing porosity adds some specific value to the phase velocity.

Finally, increase in axial and circumferential wave numbers cause considerable rise in the phase velocity. The wave numbers in the axial direction are two order of magnitude greater than circumferential wave number. Thus, at same increase in wave numbers, circumferential wave numbers have greater influence on the phase velocity.

6. Conclusions

This study performed first-order dynamic stability analysis of Small cell lung cancer structure. Governing differential motion equations were solved analytically based on Navier-solution procedure. Besides, the current small cell lung cancer structure is simulated via NSGT. Due to some imperfection of the current small cell lung cancer structure, porosity with 2 patterns was considered. Validation of the approach was carried out by comparing this study results with those published in available literature. For more verification, the outputs of current reports are compared with the results of adaptively tuned deep neural network (DNN). The numerical results revealed that:

- Curvature of the shell structure is not being important parameter in determining natural frequency of the structure.
- Increase in nonlocal parameter cause deterioration in frequency response of the structure.
- Increase in length scale parameter is in favor of vibrational behavior of the structure.
- Phase velocity reduces with increasing nonlocality.
- Independent from the value of nonlocal parameter, increasing porosity adds some specific value to the phase velocity.
- Increase in wave number results in rise in the phase velocity.

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