

Computational analysis of molecular dynamics results in a fuzzy scaled system

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Abstract. This study presents a computational analysis of molecular dynamics results within a fuzzy scaled system framework. Molecular dynamics simulations are widely used to investigate the behavior of materials at the atomic level, providing insights into their structural and dynamic properties. However, the inherent uncertainties and complexities in molecular interactions often challenge traditional analytical approaches. By applying fuzzy logic to the analysis of molecular dynamics results, we can effectively capture the variability in atomic interactions and enhance the interpretation of simulation outcomes. This approach enables the development of a more nuanced understanding of material behaviors under various conditions, accounting for factors such as temperature fluctuations and external stresses. The fuzzy scaled system allows for the integration of qualitative and quantitative data, facilitating a comprehensive assessment of molecular dynamics results. Through detailed computational experiments, we demonstrate the efficacy of the fuzzy scaled system in analyzing molecular dynamics data, highlighting its ability to improve prediction accuracy and provide meaningful insights into material properties. The findings underscore the potential of combining fuzzy logic with molecular dynamics simulations to advance the field of computational materials science. This research contributes to the development of more robust analytical tools for interpreting complex molecular behaviors, ultimately paving the way for innovations in material design and engineering applications.

Keywords: fuzzy grey GM(1,1) model; nanocomposite; nonlocal elasticity; size-dependent properties; stability

1. Introduction

Molecular dynamics (MD) simulations have become a cornerstone in the study of material properties at the atomic level, enabling researchers to explore the intricate behaviors of molecules and their interactions under various conditions. These simulations provide valuable insights into phenomena such as diffusion, phase transitions, and mechanical properties, which are critical for advancements in fields ranging from materials science to biophysics. However, despite their

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power, MD results often come with inherent uncertainties and complexities that can complicate the interpretation of data.

Traditional analytical methods may struggle to account for the variability and imprecision present in molecular dynamics simulations, particularly when dealing with large datasets or non-linear relationships. This limitation highlights the need for innovative approaches that can effectively manage uncertainty and enhance the robustness of analysis. One promising solution lies in the application of fuzzy logic, which offers a framework for handling ambiguity and imprecision in data interpretation.

This study introduces a fuzzy scaled system to analyze molecular dynamics results, integrating fuzzy logic principles with computational analysis. By employing this approach, we aim to capture the nuances of molecular interactions and provide a more comprehensive understanding of the underlying physical phenomena. The fuzzy scaled system allows for the incorporation of both qualitative and quantitative aspects of data, enabling researchers to better represent the inherent uncertainties in molecular dynamics outputs.

Through this investigation, we will explore the benefits of using a fuzzy scaled system in the context of molecular dynamics, demonstrating its potential to improve prediction accuracy and facilitate more informed decision-making in material design and analysis. By bridging the gap between fuzzy logic and molecular dynamics, this research seeks to enhance the analytical capabilities available to scientists and engineers, ultimately contributing to the development of advanced materials and innovative applications in various domains.

Therefore, the analysis of system latency is stable in research (Mori 1985, Trine Aldeen 1995, Tsai *et al.* 2012, 2015, Chen 2011, 2014) has been published and demonstrated. In recent years, there have been many interesting topics related to system administration. Numerous applications have been received successfully, some have been received. Of course, many fundamental issues still need to be resolved. And the main problem with control systems is designing systems that ensure stability. Several stability studies have recently been conducted (see Tanaka Sugeno 1992, Tim *et al.* 2021, Zhen *et al.* 2021, Chen *et al.* 2022, Hsiao *et al.* 2005, Wang *et al.* 1996, Feng *et al.* 1997 and references therein). For example, Chiang *et al.* (2001, 2002, 2004) provided a new criterion for the system, Cheng *et al.* (2002) provided IMT units for the system, Hsiao *et al.* (2003, 2005) Application of Artificial Intelligence Theory to Nonlinear Systems, Hsieh *et al.* (2006) Proposition of Stability Analysis for Artificial Intelligence, Lin *et al.* (2010). Implementation of control in the TLP system, Chen *et al.* (2006, 2007, 2009) have also demonstrated the efficiency of neural networks using LDI theory. Recently, Zhou *et al.* (2023) published studies but have not yet addressed the stability and instability problems of large systems with multiple delays. Furthermore, some promising methodologies would be better choices, On the other hand, atomic simulations show that the elastic modulus of 1-2nm diameter CNTs increases with increase in the diameter (Chang and Gao 2003). It is argued that the increase in elastic modulus in small diameter (<1.5 nm) is due to the excessive strain imposed on the graphene shells, and this effect is not prevalent in the experimental results that deal with 10-25 nm nanotubes. (Chang and Gao 2003) presented an analytical method based on molecular dynamics to calculate the elastic properties of carbon nanotubes as a function of their geometry parameters such as diameter and chirality. The results indicate that the Young modulus of SWCNT increases with increase in diameter and then converges to a constant value for large diameters. (Li and Chou 2003) calculated the young and shear modulus of single layer carbon nanotubes using a structural mechanics method. In their analysis, a C-C bond is modeled as a beam with specific Young, bending and shear moduli that were calculated by matching beam specifications with force field constants. Using this method,

they observed that the Young modulus of CNTs reduces with increase in diameter. The shear modulus also shows similar dependency on the diameter. In recent years, length dependent properties of SWCNT is investigated by (Naumov *et al.* 2013, Rao *et al.* 2015, Zhu and Li 2017, Taati *et al.* 2020) and (Ranjbartoreh and Wang 2010). Anandatheertha *et al.* (2010) used molecular dynamics based finite element method to evaluate Young modulus of SWCNT. In lengths smaller than 60 nm, the Young modulus exhibits an increase when increasing in length of the CNT, and for longer lengths, it converges to a constant value. Ranjbartoreh and Wang (2010) employed molecular dynamics simulation to predict behavior of SWCNT under various loading conditions. The results show that the Young modulus increases with increase in the length. There can be found several research works on the size dependent vibrational and buckling behavior of CNTs and CNT-reinforced nano-composites employing nonlocal and gradient theories of elasticity (Hosseini *et al.* 2017, 2018, Aydogdu *et al.* 2018, Boutaleb *et al.* 2019, Ebrahimi *et al.* 2019a, Soni *et al.* 2020). Nonlocal theory is also employed in obtaining size-dependent responses of properties other than mechanical ones. Coupled magnetic, thermal and elasticity responses in shape memory alloyed was investigated by Lata and Singh (2021, 2022)

In investigating the mechanical properties of CNTs, the classical continuum based modeling has also been adopted by many researchers (Liu *et al.* 2020a, Wang *et al.* 2020, Zhou *et al.* 2020, Dai *et al.* 2021a, Guo *et al.* 2021a, Shao *et al.* 2021, Wu and Habibi 2021, Kong *et al.* 2022). Employing classical theory of elasticity instead of atomic simulation, some complicated mechanical behavior such as vibrations and buckling of CNTs can be studied (Shariati *et al.* 2012, 2016a, b, Shariati *et al.* 2019, 2020d, e, f, g, h, i, j, 2021a, b, Fan *et al.* 2022, Luo *et al.* 2022b, Wang *et al.* 2022a, Xia *et al.* 2022). Another virtue of employing the classical theory of elasticity is that it has less computational costs than the atomic simulations. However, the classical continuum modeling cannot reflect the size dependency of properties in nano materials. In the constitutive equation of the classical continuum theory, the stress is assumed a function of the local strain, so nonlocal effects and size parameters are not observed in the equations of the classical elasticity theory. Nonlocal theory of elasticity (Eringen 1972) incorporating an internal length scale parameter into the constitutive equation, presents size-dependent mechanical properties in nano materials (Zenkour and Abouelregal 2015, Lata and Singh 2019, Pham *et al.* 2021). Pisano and Fuschi (2003) presented a nonlocal formulation for a bar under uniaxial tension and their results indicated a non-uniform strain distribution in the bar. Failla *et al.* (2010) used approximate methods in order to obtain strain, displacement and strain energy in a nonlocal bar under uniaxial tension. After (Peddieson *et al.* 2003), the size dependent nonlocal theory of elasticity has been widely used in predicting mechanical behavior of nanomaterials. They formulated the deflection equation of a nonlocal Bernoulli-Euler beam, and showed that based on the nonlocal elasticity theory, the nonlocal effect manifest itself in the nano-scale devices. Sudak (2003) investigated the buckling of a multiwall carbon nanotube (MWCNT) using nonlocal elasticity theory. In the analysis, each individual CNT is modeled as a column and the buckling of the MWCNT is investigated by considering the interaction between adjacent CNTs as van der Waals interaction. The results demonstrated that the critical load of buckling is highly dependent on the scale parameter. In these studies, the results of the nonlocal elasticity are more conservative than those of the classical elasticity. Wang *et al.* (2006) investigated buckling of CNTs using both nonlocal column and shell models. In the nonlocal shell model, the critical load is found to be function of diameter as well as length of the CNT, where the column model cannot reflect the dependency of critical load on the diameter. Zhang *et al.* (2005) investigated free vibrations of DWCNT using nonlocal elasticity theory. Each CNT was modeled as a nonlocal beam and the

interaction between two CNT is modeled as spring with a specific coefficient. They concluded that the classical theory of elasticity could overestimate the amount of the natural frequencies.

In nanocomposite materials, which are frequently reinforced with CNTs and other nanostructures, elasticity parameters are usually considered as constants (Bellal *et al.* 2020, Matouk *et al.* 2020, Rouabhia *et al.* 2020, Bouafia *et al.* 2021, Heidari *et al.* 2021, Kumar *et al.* 2021, Van Vinh and Tounsi 2021, Bendaida *et al.* 2022). However, a size dependent properties are more desirable in this context. Using embedded size-dependent theories in analyzing nanocomposite puts extra computational costs in calculation which could be easily avoided using approximate or exact closed-form relations (Al-Furjan *et al.* 2020h, i, 2021, Bendenia *et al.* 2020, Arshid *et al.* 2021, Huang *et al.* 2021d, Zerrouki *et al.* 2021). On the other hand, in chemical production of nanostructures, it is barely possible to control size of each nanostructure (Al-Furjan *et al.* 2020g, Bourada *et al.* 2020, Bousahla Abdelmoumen *et al.* 2020, Asgharnejad Lamraski *et al.* 2022, Moradi *et al.* 2022a, b, Vatanpour *et al.* 2022a, b). Moreover, novel methods of evaluating size and effects of nanostructures and nanoparticles are commonly relies on statistical approximations (Lingamdinne *et al.* 2023). Using numerical methods like finite element has its own drawbacks in terms of computational, accuracy and modeling time (Amelirad and Assempour 2019, 2021).

Thus, this study provides a stability formula based directly on Lyapunov's method, which provides asymptotic stability for large multi-delay systems. According to this explanation and limited control system, fuzzy control groups are involved in stabilizing large-scale systems in multi-delay systems with many interconnected systems. Furthermore, these subsystems are represented in the models by a simple Takagi-Sugen law model. Each of these layers is represented by a linear model of the system. Therefore, the linear control response can be used as a fixed response. Therefore, the coverage design type based on the fuzzy model is the Parallel Distributed Coverage (PDC) model. Lines in all linear spaces use the same assumptions. and we highlight the results that show the best performance of the proposed damage propagation theory for the structural analysis of composites in space.

The stability measurements are obtained and verified using the Lyapunov method to ensure the asymptotic stability of the multi-delay system, and we highlight the results that show the best performance of the proposed damage propagation theory for the analysis of complex land structures. Finally, descriptive results and conclusions for the numerical model are presented.

2. Nonlocal theory of elasticity

Nonlocal theory of elasticity is one the theories that take into account the effects of the size in the mechanical properties (Ma *et al.* 2022, Zhao *et al.* 2022, Hou *et al.* 2021, Huang *et al.* 2021b, c, Jiao *et al.* 2021, Liu *et al.* 2021c, Moradi *et al.* 2021, Xu *et al.* 2021, Dong *et al.* 2022, Fan *et al.* 2022, Luo *et al.* 2022a, b, Michael *et al.* 2022, Wang *et al.* 2022b, c, Yang *et al.* 2022a, b, Yu *et al.* 2022, Zheng *et al.* 2022, Zhu *et al.* 2022). The essence of incorporating size effects in the mechanical properties is that the stress at a point of the material is considered to be affected by not only the local strain but also the nonlocal strain field. The influence of the nonlocal strain is imposed on the stress by employing an attenuation function. In this way, strain at farther points (compared to internal characteristic length) has less influence on the stress than strain at the points near the reference point. The constitutive equation of a nonlocal linear homogenous elastic solid is given as follows:

$$F^0 = (F_1^0, F_2^0, \dots, F_n^0) \quad (1)$$

where σ_{ij} are the nonlocal stress components, and ε_{ij} are the strain components for infinitesimal displacement components, and they are defined by the following equation:

$$F^1 = (F_1^1, F_2^1, \dots, F_n^1), \quad (2)$$

where u_i are the displacement vector components. The fourth order tensor C_{ijkl} is the elasticity tensor of the classical elasticity (Fan *et al.* 2022, Luo *et al.* 2022b, Wang *et al.* 2022a, Xia *et al.* 2022).

As mentioned above, the influence of the nonlocal strain on the stress at point \mathbf{x} is incorporated by an attenuation function $\alpha(|\mathbf{x}-\mathbf{x}'|)$. The attenuation function $\alpha(|\mathbf{x}-\mathbf{x}'|)$ is a positive scalar function of the Euclidean distance between point \mathbf{x}' and the reference point \mathbf{x} . When the Euclidean distance is very large compared to internal length $|\mathbf{x}-\mathbf{x}'| \rightarrow \infty$ the attenuation function vanishes $\alpha \rightarrow 0$. However, in practice, the influence of nonlocal strain after a specific distance, called influence distance, vanishes, so that the attenuation function after that distance becomes $\alpha(|\mathbf{x}-\mathbf{x}'|) \approx 0$ (Polizzotto 2001). For small distances, the value of the attenuation function α is considerable whereas at large distances the nonlocality effects substantially decrease. The influence distance is characterized by the internal characteristic length, and it is in the same order of the internal characteristic length. It is expected when the influence distance vanishes so that only local strain takes into account, the constitutive Eq. (1) becomes the local form of:

$$\frac{dF^1}{dt} + aF^1 = b, \quad (3)$$

where a represents the expanded coefficient which needs to be a non-negative value to have a stable dynamic, b represents the control variable Gray, both unknown variables.

The first order of differential equations, dF^1/dt is denoted by

$$\frac{dF^1}{dt} = \lim_{h \rightarrow 0} \frac{F_{t+h}^1 - F_t^1}{h}, \quad \forall t \geq 1. \quad (4)$$

Let Δt be the unit sampling interval, then the difference of the generation series F^1 can be described as a discrete time series $F_{t+1}^1, \forall t \geq 1$ which

$$\frac{dF^1}{dt} = \frac{F_{t+1}^1 - F_t^1}{\Delta t} = F_{t+1}^1 - F_t^1 = F_{t+1}^0, \quad \forall t \geq 1. \quad (5)$$

Approximation in (5) and therein equations lie in the linear assumptions. The second part of the first-order gray model is the mean F_t^1 and F_{t-1}^1 . Then we can rewrite equation (3) as

$$F_{t+1}^0 = a \left[-\frac{1}{2}(F_{t+1}^1 + F_t^1) \right] + b, \quad \forall t \geq 1. \quad (6)$$

If $t = 1, 2, \dots, n$, then equation (6) can be rewritten in matrix form as

$$\begin{bmatrix} F_2^0 \\ F_3^0 \\ \vdots \\ F_n^0 \end{bmatrix} = \begin{bmatrix} -\frac{1}{2}(F_2^1 + F_1^1) & 1 \\ -\frac{1}{2}(F_3^1 + F_2^1) & 1 \\ \vdots & \vdots \\ -\frac{1}{2}(F_n^1 + F_{n-1}^1) & 1 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix}. \quad (7)$$

Using the least squares method, the variables a and b in equation (7) can be solved as

$$\hat{a} = \begin{bmatrix} a \\ b \end{bmatrix} = (B^T B)^{-1} B^T F^0 \quad (8)$$

where the states

$$F_0 = \begin{bmatrix} F_2^0 \\ F_3^0 \\ \vdots \\ F_n^0 \end{bmatrix}, \quad B = \begin{bmatrix} -\frac{1}{2}(F_2^1 + F_1^1) & 1 \\ -\frac{1}{2}(F_3^1 + F_2^1) & 1 \\ \vdots & \vdots \\ -\frac{1}{2}(F_n^1 + F_{n-1}^1) & 1 \end{bmatrix}.$$

By obtaining the solutions of the variables a and the matrix bi (8), we can solve the differential equation (3) to obtain the F_{t+1}^1 estimated cumulative value at

$$\hat{F}_{t+1}^1 = \left(F_1^0 - \frac{b}{a}\right) e^{-at} + \frac{b}{a}, \quad \forall t \geq 1. \quad (9)$$

Finally, it is possible to obtain a forecast value for period $t+1$ which

$$\hat{F}_{t+1}^0 = \hat{F}_{t+1}^1 - \hat{F}_t^1, \quad \forall t \geq 1. \quad (10)$$

Suppose that the original series with fuzzy data F^{0*} is defined as

$$\hat{F}_t^{0,R} = \hat{F}_t^{1,R} - \hat{F}_{t-1}^{1,R}, \quad \forall t \geq 2 \quad (11)$$

You can get $\tilde{F}_1^{0*}, \tilde{F}_2^{0*}, \dots, \tilde{F}_n^{0*}$ explained fuzzy values $\hat{F}_{n+1}^0, \hat{F}_{n+2}^0, \dots, \hat{F}_{n+k}^0, \forall t \geq 1$ through the input data. Theorem 1 shows that a fuzzy number $\hat{F}_t^1, \forall t \geq 2$ is not a symmetric fuzzy number, so \hat{F}_t^0 it is also not a symmetric fuzzy number. Conversely, \hat{F}_t^0 to estimate the forecast error, the mean is defined as $\hat{F}_t^{0,Aver}$, given by

$$\hat{F}_t^{0,Aver} = \frac{F_t^{0,L} + F_t^{0,R}}{2}, \quad \forall t \geq 2.$$

Therefore, the gray time series model GM(1,1) is used. F_2^0, \dots, F_n^0 is specified to extrapolate the values for $\hat{F}_{t+1}^0, \hat{F}_{t+2}^0, \dots, \hat{F}_{t+k}^0, \forall k \geq 1$. The main features of the Takagi-Sugeno multilayer fuzzy model are the expression of each rule by a linear equation of state, and the model is as follows (Chen 2014, Chen *et al.* 2019, 2020):

r_j is the IF-THEN rule number for this $A_{ij} j$. *Subsystem.*, $A_{i \leftrightarrow k \leftrightarrow j}$ and B_{ij} are paired system matrices, state $x_j(t)$, input $u_j(t)$, $\tau_{k \leftrightarrow j}$ delay fuzzy set M_{ipj} ($p = 1, 2, \dots, g$) and assumption are used $x_{1j}(t) \sim x_{gj}(t)$ to derive the dynamic fuzzy model:

$$\begin{aligned} \dot{x}_j(t) &= \frac{\sum_{i=1}^{r_j} w_{ij}(t) \left\{ A_{ij} x_j(t) + \sum_{k=1}^{N_j} A_{i \leftrightarrow k \leftrightarrow j} x(t - \tau_{k \leftrightarrow j}) + B_{ij} u_j(t) \right\}}{\sum_{i=1}^{r_j} w_{ij}(t)} \\ &= \sum_{i=1}^{r_j} h_{ij}(t) \left\{ A_{ij} x_j(t) + \sum_{k=1}^{N_j} A_{i \leftrightarrow k \leftrightarrow j} x(t - \tau_{k \leftrightarrow j}) + B_{ij} u_j(t) \right\} \end{aligned}$$

with

$$w_{ij}(t) = \prod_{p=1}^g M_{ipj}(x_{pj}(t)), \quad h_{ij}(t) = \frac{w_{ij}(t)}{\sum_{i=1}^{r_j} w_{ij}(t)} \quad (12)$$

where $x_{pj}(t) w_{ij}(t) \geq 0$, $i = 1, 2, \dots, r_j$ and $\sum_{i=1}^{r_j} w_{ij}(t) > 0$, $i = 1, 2, \dots, r_j$, $\sum_{i=1}^{r_j} h_{ij}(t) = 1$.

3. Smart control for nonlocal elastic bar in tension

In this section, we consider an SWCNT with length L under uniaxial tension. For simplicity, the CNT is modeled as a one-dimensional nonlocal bar in tension under applied stress $\bar{\sigma}$, and one end of it is pinned at ($x=0$). From equilibrium of the bar, it is concluded that the internal stress of the CNT is uniform and equals the applied stress $\bar{\sigma}$. The one-dimensional form of Eqs. (9) and (2) is as Eqs. (11) and (12), respectively:

$$\varepsilon(x) = \frac{\bar{\sigma}}{\zeta_1 E} - \frac{\zeta_2}{\zeta_1} \int_0^L \bar{\alpha}(|x - x'|) \varepsilon(x') dx' \quad (13)$$

This equation is the Fredholm equation of the second kind and it is indicated that, despite the fact that the stress state in the CNT is uniform, the strain is not uniform in the CNT. A solution for this equation with following form for attenuation function $\bar{\alpha}$ is given by (Pisano and Fuschi 2003).

$$\bar{\alpha}(r) = A \exp\left(-\frac{r}{l}\right) \quad (14)$$

And, the solution for Eq. (13) is given by the following equation (Pisano and Fuschi 2003):

$$\varepsilon(x) = \frac{\bar{\sigma}}{E} \left\{ 1 + \frac{\zeta_2}{4\zeta_1} \left[e^{\frac{x}{l}(\frac{\zeta_2}{2\zeta_1}+1)} + e^{\frac{L-x}{l}(\frac{\zeta_2}{2\zeta_1}+1)} \right] \right\} \quad (15)$$

Using Eq. (15) and integrating Eq. (12) the displacement for each point is obtained:

and

$$andu(x) = \frac{\bar{\sigma}L}{E} \left\{ \frac{x}{L} - \frac{l}{L} \frac{\frac{\zeta_2}{2\zeta_1}}{2\left(\frac{\zeta_2}{2\zeta_1}+1\right)} \times \left[e^{\frac{x}{l}(\frac{\zeta_2}{2\zeta_1}+1)} - e^{\frac{L-x}{l}(\frac{\zeta_2}{2\zeta_1}+1)} + e^{\frac{l}{l}(\frac{\zeta_2}{2\zeta_1}+1)} - 1 \right] \right\} \quad (16)$$

In order to calculate the Young modulus of the CNT, the applied stress is divided by the average strain inside the bar. The average strain of the CNT is obtained by following relation.

$$\varepsilon_{ave\ and} = \frac{1}{L} \int_0^L \varepsilon(x) dx = \frac{u(L)}{L} \quad (17)$$

$$and = \bar{\varepsilon} \left\{ 1 - \frac{l}{L} \frac{\frac{\zeta_2}{2\zeta_1}}{\left(\frac{\zeta_2}{2\zeta_1}+1\right)} \left[e^{-\frac{L}{l}(\frac{\zeta_2}{2\zeta_1}+1)} - 1 \right] \right\}$$

where the $\bar{\varepsilon}$ is the strain field produced with considering the classical constitutive equation that is $\bar{\varepsilon} = \bar{\sigma}/E$. Finally, the Young modulus of the CNT can be obtained as follows:

$$\frac{E^{nl}}{E} = \left\{ 1 - \frac{l}{L} \frac{\frac{\zeta_2}{2\zeta_1}}{\left(\frac{\zeta_2}{2\zeta_1}+1\right)} \left[e^{-\frac{L}{l}(\frac{\zeta_2}{2\zeta_1}+1)} - 1 \right] \right\}^{-1} \quad (18)$$

Theorem 1: The fuzzy large-scale system F is asymptotically stable, if the feedback gains (K_{ij}) are chosen to satisfy $\beta_j = \sum_{\substack{n=1 \\ n \neq j}}^J (\|C_{nj}^T P_j\| + \|C_{jn}^T P_n\|) > 0$, for $j=1, 2, \dots, J$ with

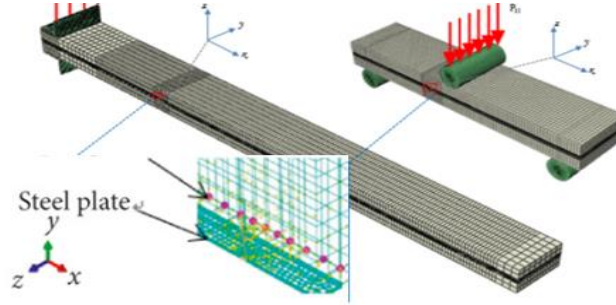


Fig. 1 Finite element model of an aluminum beam

$$G_{ifj} = \frac{(A_{ij} - B_{ij}K_{fj}) + (A_{fj} - B_{fj}K_{ij})}{2}, \quad P_j = P_j^T > 0, \quad \text{and } \lambda_m(Q_{ij}) \text{ as well as } \lambda_m(Q_{ifj})$$

denote the minimum eigenvalues of Q_{ij} and Q_{ifj} , respectively.

4. Example

ANSYS finite element (FE) software has an electromechanical stress simulation function that can simulate aluminum beams with customized boundary conditions. In the finite element model the beam is in SOLID185 unit and the PZT sensor is in SOLID5 unit.

The final model of the aluminum beam is very similar to the data of Liu and Jiang (2009) (Fig. 1). Aluminum support sample size is 1000 x 20 x 2 mm, 50 × 10 × PZT detector is placed. 0.5 mm to the left of the 62.5 mm beam. Two cracks of length 3 mm and 6 mm of length 500 mm are visible from the left of the beam. The excitation voltage of the PZT sensor is 4 V. Numerical simulations were performed in three cases: an aluminum beam without cracks, 3 mm cracked aluminum beam and 6 mm cracked aluminum beam. Calculate the frequency range.

For all cases, the number of maximum frequencies in this study is the same as Liu and Jiang (2009), there is no crack. Two panels had 3 mm cracks and three panels had 6 mm cracks. However, there were two patterns in each of these three cases. The maximum resistance in this study deviates from the maximum value of Liu and Jiang (2009), and the deviation is less than 1% and can be ignored in the comparison (Table 3). This study demonstrates the high accuracy and reliability of barrier response simulation. Therefore, the numerical simulation results are used for the structural crack detection problem.

This chapter presents a detailed review of crack analysis in beams. The selection of frequency range is very important for impedance-based error analysis. Several studies have shown that the properties of resonance barriers are more sensitive to structural damage. Ryu *et al.* (2017) measured the impedance response in the frequency range 10–55 kHz. The highest frequency range is 24–26 kHz. Ai *et al.* (2018) measured the impedance response. Frequency range 10–55 kHz. The highest frequency range is 24–26 kHz. Ai *et al.* (2017). According to 0–300 kHz (2018). This reduces the sensitivity of the RMSD index. Damage in this study the response of uncracked, 3 mm cracked, and 6 mm cracked barriers was studied at the following frequency ranges: 10 to 100 kHz (frequency step 0.1 kHz) Fig. 2 shows the simulated impedance response for the three case studies. It should be noted that there are several distinct amplitude impedance peaks in this frequency

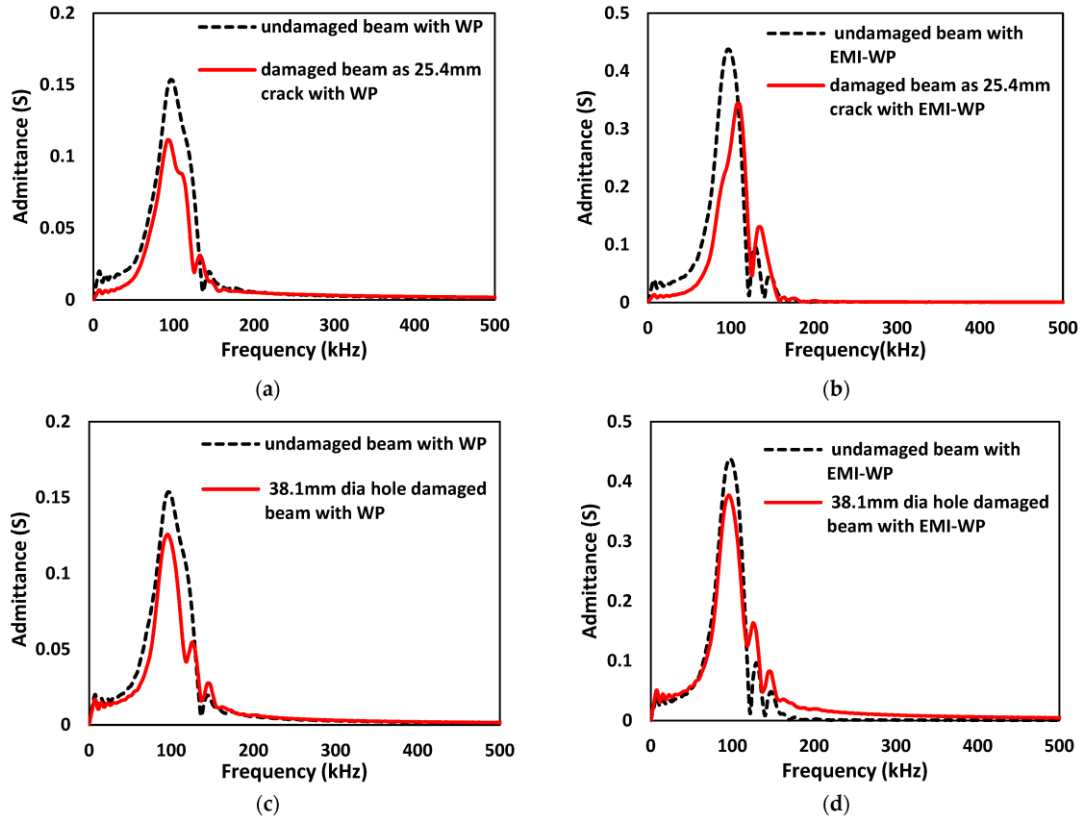


Fig. 2 EMI response of aluminum beam with different cracks

range. The impedance response is then divided into 18 subbands (eg 10-15 kHz, ..., 95-100 kHz) with a magnitude of 5 kHz. The RMSD index is calculated according to formula (1) (3) applied to 18 subbands, so the most sensitive subband is selected as input to the next step of MLP-DNN.

Different parts of the frequency range have different RMSD indices for the same damage condition. Furthermore, different damage conditions may result in different RMSD ratios, even if they are in the same sub-frequency range. There is no specific rule for changing the RMSD index. For example, in the 10–15 kHz sub-frequency range, the RMSD factor decreases with increasing crack. However, in the 15–20 kHz sub-frequency range, the RMSD factor decreases with a growing crack. In the frequency range of 45–55 kHz, the RMSD coefficient reaches its maximum value and is higher than that of other frequency sub-ranges. This is also the frequency range where the resonant impedance peak in the response is highest. Therefore, the RMSD index can predict the cracks in the beam. However, the RMSD index cannot determine the crack size. Therefore, MLP DNN was used to determine the crack size of the beam.

Two additional crack conditions are proposed for the size of the crack: 2 mm crack and 5 mm crack, so the training arm will not crack or break.

This problem uses a frequency range of 45 to 55 kHz with a frequency step of 0.01 kHz. Fig. 3 shows the electronic response. MPedance or DNN MLP input data, the crack size analysis results are summarized in Fig. 4 for the training case. The accuracy of crack size analysis results is 100% under specified operating conditions. Crack size results were 98.5% accurate for 2 mm

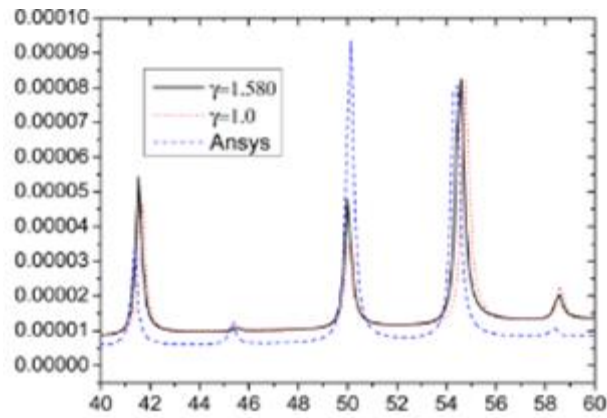


Fig. 3 EMI response during crack prediction

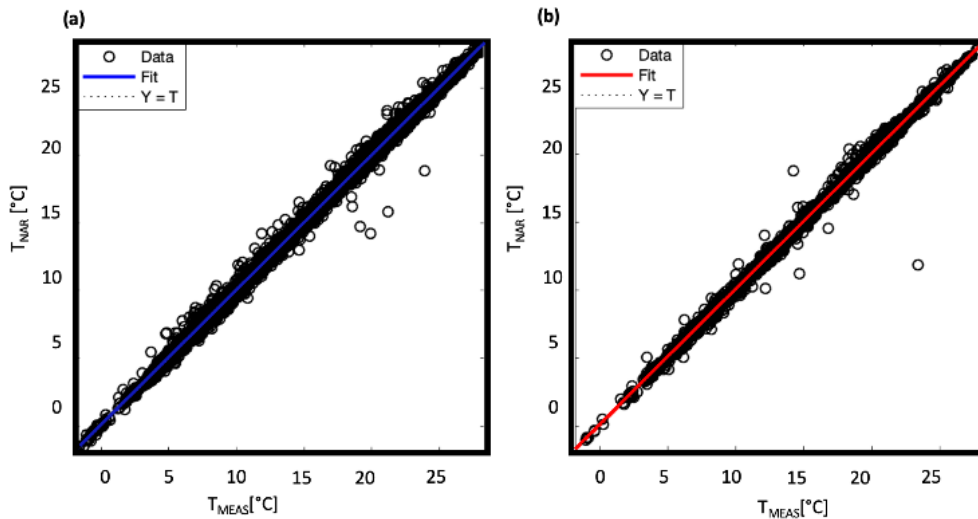


Fig. 4 Crack size prediction results of MLP ANN

Table 1 Performance comparison of different prediction models

Way	RMS error (training)		RMS error (experimental)		CPU time (training)	
	Average	Deviation	Average	Deviation	Average	Deviation
EA's suggestion	5.4	0.4	5.6	0.7	113.2	4.8
(Koza 1992) Details	28.3	3.5	30.2	4.2.2	143.5	6.5
(Vogel 1994) Author	19.5	1.5	20.1	4.3	257.2	8.5
(Rechenberg 1994) Author	14.7	1.7	16.2	2.1	216.3	9.2.2

cracks and 95.6% accurate for 5 mm cracks, allowing MLP to determine crack size with very high accuracy.

The quality values of the vibration control system of the offshore facility are $R = 10^{-5}$ and $N = 210/T$. Networking between distributed devices and offshore networks differs from traditional

point control mechanisms. Due to the extreme conditions, delays and loss of packages are usually unavoidable.

The upper bounds on the delay are $m_{sc} = 0.7/T = 70$ and $m_{ca} = 0.7/T = 70$. $M = 140$, which is considered the maximum delay in ocean engineering. Based on the above variables, we obtained the following simulation results with different values of packet loss m_1 and m_2 .

Table 1 shows these comparative performances of the genetic algorithm during the training and testing phases, including the mean and standard deviation of the RMS error and CPU time. As the table shows, the EA not only consumes less CPU time during the training and testing phases, but also produces less RMS error compared to other methods.

5. Conclusions

Based on earlier experiments and simulations the mechanical properties of nanomaterials such as carbon nanotubes are strongly dependent on length scales. The classical elasticity theory, because of its intrinsic nature, cannot present a size dependent result. In this paper, using nonlocal theory of elasticity, dependency of Young elasticity modulus of CNT on the length was investigated. The size exact size dependent of CNTs are often calculated from molecular dynamics simulation. According to the study, there is a fundamental relationship between the fuzzy method and the Gray method to solve the forecasting problem with powerful short-term forecasting models. We highlight results that demonstrate the high performance of the proposed theory applied to damage propagation for structural analysis of aircraft composites.

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